# Supporting Information for: Mutual diffusivities of mixtures of carbon dioxide and hydrogen and their solubilities in brine: Insight from molecular simulations

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#### <sup>50</sup> S1 Mixture Densities for H<sub>2</sub>-CO<sub>2</sub> mixtures

### <sup>51</sup> S1.1 Preparation of systems for production runs in the NVE <sup>52</sup> ensemble

The procedure to prepare systems for production runs in the NVE ensemble using systems 53 consisting of 2000 molecules is described below. To avoid overlaps between molecules, binary 54 mixtures of H<sub>2</sub> and CO<sub>2</sub>, simulated as rigid bodies, are placed inside a large cubic simulation 55 box ( $\approx 100$  Å). Simulations of 2000 molecules are performed in the isotropic version of the 56 NPT ensemble using the Nosé-Hoover barostat and thermostat as described originally by 57 Martvna et al.<sup>1</sup> and Kamberaj et al.<sup>2</sup>, using damping constants of 1 and 0.1 ps, respectively. 58 In the initialization phase, the time-step is gradually increased from  $10^{-4}$  (fs) towards a final 59 value of 0.5 fs, to allow the system to relax towards equilibrium. Following the initialization 60 phase lasting 12.5 ps, a production phase lasting 250 ps ensues during which the density of 61 the system is recorded every time step. The NPT production phase is followed by a short 62 simulation in the NVT ensemble lasting 50 ps. In this phase, the size of the simulation box 63 is uniformly scaled at a constant rate, until it reaches a size that aligns with the average 64 density obtained in the NPT production phase. The simulations are continued with a fixed 65 box size for 25 ps (initialization phase) and 250 ps (production phase) in the NVT ensemble, 66 where the Nosé-Hoover thermostat is used with a damping constant of 0.1 ps. During the 67 production phase in the NVT ensemble, the average total energy is calculated, which is then 68 used to scale the molecule velocities to achieve a desired temperature in the NVE ensemble. 69 After scaling the velocities of all molecules, the system is simulated in the NVE ensemble 70 for 25 ps (initialization phase) and 250 ps (production phase). During the production phase 71 the temperature, pressure and the total energy of the system are recorded and checked for 72 conservation. The raw data for the simulations of the larger systems are provided in Table S2. 73

#### <sup>74</sup> S1.2 Mixture density vs mixture composition

<sup>75</sup> H<sub>2</sub>-CO<sub>2</sub> mixture densities for p between 10 and 45 MPa, and T between 323.15 and 423.15 K, <sup>76</sup> in increments of 25 K are plotted in Figs. S1-S2. Average densities obtained from MD <sup>77</sup> simulations in the *NPT* ensemble (symbols), are compared to the corresponding values from <sup>78</sup> the thermodynamic database REFPROP<sup>3</sup> (solid lines).



Figure S1: H<sub>2</sub>-CO<sub>2</sub> mixture densities ( $\rho$ ) at 10, 15, 20 and 30 MPa as a function of the hydrogen mole fraction  $x_{\rm H_2}$ , and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Error bars are smaller than the symbols. Lines are colored as per the legend in subfigure (a).



Figure S2: H<sub>2</sub>-CO<sub>2</sub> mixture densities ( $\rho$ ) at 35, 40, and 45 MPa as a function of the hydrogen mole fraction  $x_{\text{H}_2}$ , and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Error bars are smaller than the symbols. Lines are colored as per the legend in subfigure (a). See the caption of Fig. S1.



<sup>79</sup> S1.3 Mixture density vs pressure

Figure S3: H<sub>2</sub>-CO<sub>2</sub> mixture densities ( $\rho$ ) for different hydrogen mole fractions between 0 and 0.5, as a function of the pressure p, and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Error bars are smaller than the symbols. Lines are colored as per the legend in subfigure (a).



Figure S4: H<sub>2</sub>-CO<sub>2</sub> mixture densities ( $\rho$ ) for different hydrogen mole fractions between 0.6 and 1, as a function of the pressure p, and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Error bars are smaller than the symbols. Lines are colored as per the legend in subfigure (a). See the caption of Fig. S3.

#### <sup>80</sup> S1.4 Relative deviations between simulations and REFPROP

Relative deviations, expressed as percentage, between the densities computed from MD simulations in the NPT ensemble and those acquired from the REFPROP<sup>3</sup> database are displayed in Figs. S5-S7.



Figure S5: Relative deviations of the  $\text{CO}_2$ -H<sub>2</sub> mixture densities obtained from MD simulations ( $\rho^{\text{MD}}$ ) from the REFPROP<sup>3</sup> database ( $\rho^{\text{RFP}}$ ), plotted for  $p \in [5, 15]$  MPa, as a function of  $x_{\text{H}_2}$  in the mixture. At each pressure the symbols are color coded (see Fig. S1) for T between 323.15 K and 423.15 K. The grey dashed lines indicate deviations of  $\pm 5\%$ .



Figure S6: Relative deviations of the  $\text{CO}_2$ -H<sub>2</sub> mixture densities obtained from MD simulations ( $\rho^{\text{MD}}$ ) from the REFPROP<sup>3</sup> database ( $\rho^{\text{RFP}}$ ), plotted for  $p \in [20, 30]$  MPa, as a function of  $x_{\text{H}_2}$  in the mixture. At each pressure the symbols are color coded (see Fig. S1) for T between 323.15 K and 423.15 K. The grey dashed lines indicate deviations of  $\pm 5\%$ . See Fig. S5.



Figure S7: Relative deviations of the  $\text{CO}_2$ -H<sub>2</sub> mixture densities obtained from MD simulations ( $\rho^{\text{MD}}$ ) from the REFPROP<sup>3</sup> database ( $\rho^{\text{RFP}}$ ), plotted for  $p \in [5, 15]$  MPa, as a function of  $x_{\text{H}_2}$  in the mixture. At each pressure the symbols are color coded (see Fig. S1) for T between 323.15 K and 423.15 K. The grey dashed lines indicate deviations of  $\pm 5\%$ . See Fig. S5.

## <sup>84</sup> S2 Compressibility Factors for $H_2$ -CO<sub>2</sub> mixtures

The compressibility factor Z of a mixture is defined as,

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$$Z = \frac{pV}{N_{\text{tot}}k_BT} \tag{S1}$$

where p is the pressure, V is the average volume of the simulation box,  $N_{\text{tot}}$  is the total number of molecules in the simulation box,  $k_B$  is the Boltzmann constant, and T is the absolute temperature. The variation of Z with p is plotted in Figs. S8-S9, and  $Z(x_{\text{H}_2})$  is shown in Fig. S10.



Figure S8: Compressibility factors (Z) of H<sub>2</sub>-CO<sub>2</sub> mixtures for  $x_{H_2} \in [0, 0.4]$  and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP predictions (lines). Error bars are smaller than the symbols. Lines are colored according to the legend in subfigure (e).



Figure S9: Compressibility factors (Z) of H<sub>2</sub>-CO<sub>2</sub> mixtures for  $x_{H_2} \in [0.5, 1]$  and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) are REFPROP predictions (lines). Error bars smaller than the symbols. Lines are colored according to the legend in subfigure (e). See Fig. S8.



Figure S10: Compressibility factors (Z) of H<sub>2</sub>-CO<sub>2</sub> mixtures plotted as a function of  $x_{\rm H_2}$ . Comparison between MD simulations (symbols) are REFPROP predictions (lines). Error bars smaller than the symbols. Lines are colored according to the legend in subfigure (a). See also Figs. S8 and S9.

#### <sup>91</sup> S3 Viscosities of H<sub>2</sub>-CO<sub>2</sub> mixtures

The viscosities are computed from the time integral of the autocorrelation function of all components of the traceless pressure tensor<sup>4</sup>,

$$\eta = \lim_{t \to \infty} \left[ \frac{1}{10 \cdot 2t} \frac{V}{k_B T} \left\langle \sum_{\alpha \beta} \left( \int_0^t dt' p_{\alpha \beta}^{\text{Tr}}(t') \right)^2 \right\rangle \right]$$
(S2)

$$p_{\alpha\beta}^{\rm Tr} = \frac{p_{\alpha\beta} + p_{\beta\alpha}}{2} - \delta_{\alpha\beta} \left(\frac{1}{3}\sum_{k} p_{kk}\right) \tag{S3}$$

<sup>92</sup> where t is time, V is the volume of the simulation box,  $k_B$  is the Boltzmann constant, T <sup>93</sup> is the temperature,  $p_{\alpha\beta}^{\text{Tr}}$  are the components of a traceless tensor derived from the pressure <sup>94</sup> tensor  $p_{\alpha\beta}$  using Eq. S3,  $\delta_{\alpha\beta}$  is the Kronecker delta, and  $\langle \cdots \rangle$  indicates an ensemble average. <sup>95</sup>  $\eta$  is calculated by evaluating the slope of the linear segment of the so-called mean-square <sup>96</sup> displacement, shown within the brackets  $[\cdots]$  in Eq. S2. For calculation of viscosities, the <sup>97</sup> mean square displacements of Eq. S2 are plotted on a log-log scale as a function of time, and <sup>98</sup> the segment with a slope between 0.99 and 1.01 is chosen for computing  $\eta$ , see Fig. S11.

#### <sup>99</sup> S3.1 Determination of viscosities from MD simulations



Figure S11: (a) Mean-squared displacements (symbols) of  $\eta$  (MSD<sub> $\eta$ </sub>) calculated using Eq. S2, as a function of time for pure CO<sub>2</sub> at 50 MPa and 323.15 K. The black dashed line is a linear fit of the data within the highlighted region in red. (b) Slopes of the MSDs, calculated using 10 successive points, of the points falling within the shaded region have a slope between 0.99 and 1, and are used for the calculation of viscosities. We follow the same procedure to calculate viscosities of mixtures.



<sup>100</sup> S3.2 Viscosity vs mixture composition

Figure S12: H<sub>2</sub>-CO<sub>2</sub> mixture viscosities ( $\eta$ ) at 10, 15, 20 and 30 MPa as a function of the hydrogen mole fraction  $x_{\rm H_2}$ , and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Error bars are smaller than the symbols. Lines are colored as per the legend in subfigure (b).



Figure S13: H<sub>2</sub>-CO<sub>2</sub> mixture viscosities ( $\eta$ ) at 35, 40, and 45 MPa as a function of the hydrogen mole fraction  $x_{\rm H_2}$ , and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Error bars are smaller than the symbols. Lines are colored as per the legend in subfigure (a). See Fig. S12.



Figure S14:  $H_2$ -CO<sub>2</sub> mixture viscosities ( $\eta$ ) for different hydrogen mole fractions between 0.1 and 0.4, as a function of the pressure p, and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Lines are colored as per the legend in subfigure (a).



Figure S15: H<sub>2</sub>-CO<sub>2</sub> mixture viscosities ( $\eta$ ) for different hydrogen mole fractions between 0.6 and 1, as a function of the pressure p, and temperatures between 323.15 K and 423.15 K. Comparison between MD simulations (symbols) and REFPROP<sup>3</sup> (solid lines). Lines are colored as per the legend in subfigure (a). See Fig. S14.

#### <sup>102</sup> S4 Self-diffusion coefficients

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<sup>103</sup> The self diffusivity of the  $i^{\text{th}}$  species as calculated in an MD simulation is given by <sup>4–6</sup>,

$$D_{i}^{\text{self,MD}} = \lim_{t \to \infty} \frac{\mathrm{d}}{\mathrm{dt}} \left[ \frac{1}{6N_{i}} \left\langle \sum_{j=1}^{N_{i}} \left( \mathbf{r}_{j,i}(t) - \mathbf{r}_{j,i}(0) \right)^{2} \right\rangle \right]$$
(S4)

where  $N_i$  is the number of molecules of type i,  $\mathbf{r}_{j,i}$  is the position vector of the  $j^{\text{th}}$  molecule at time t, and the diffusion coefficient in the three orthogonal directions x, y and z each contributes a factor 2 in the denominator.

<sup>108</sup> S4.1 Determination of self-diffusion coefficients from MD simula-

109 tions



Figure S16: (a) Mean-squared displacements (symbols) of  $H_2$  (MSD), computed as per Eq. S4, as a function of time for  $H_2$  in an equimolar mixture of CO<sub>2</sub> and  $H_2$  at 50 MPa and 323.15 K. The green dashed line represents the square of the box length 22.97 Å, indicating a complete box traversal. The black dashed line is a linear fit based on data points within the red region. (b) Slopes of the MSDs, calculated using 10 successive points, of the points falling within the shaded region have a slope between 0.99 and 1, and are used for the calculation of self-diffusivities.

#### <sup>110</sup> S4.2 Finite system-size effects for $D^{\text{self}}$

Based on the density of the system, the self-diffusion coefficients are corrected for the finitesize effects using the Yeh-Hummer correction term  $D^{\text{YH}7,8}$ ,

$$D_i^{\text{self}} = D_i^{\text{self,MD}} + D^{\text{YH}}(T,\eta,L) = D_i^{\text{self,MD}} + \frac{k_B T \xi}{6\pi \eta L}$$
(S5)

where  $D_i^{\text{self}}$  is the finite-size corrected self diffusivity of the  $i^{\text{th}}$  species,  $\xi$  is a dimensionless 114 constant equal to 2.837298, and L is the box length of a cubic simulation box whose volume is 115 V. Similar to the calculation of  $\eta$ , the segment of the molecular mean-square displacements 116 with a slope between 0.99 and 1.01 on a log-log plot is chosen for the calculation of  $D_i^{\text{self}}$ , 117 see Fig. S16. As pointed out by Moultos *et al.*<sup>9</sup> the Yeh-Hummer correction to  $D_i^{\text{self,MD}}$  is 118 significant for dense systems and can be neglected otherwise, as will be shown in a subsequent 119 section. Self-diffusion coefficients are corrected for finite sizes as per Eq. S5, if the correction 120 is larger than 1% percent of  $D_i^{\text{self,MD}}$ . 121

In Figs. S17 and S18,  $D^{\text{self}}$  of H<sub>2</sub> and CO<sub>2</sub> are plotted as a function of  $N_{\text{tot}}^{-\frac{1}{3}}$ , since the size of the simulation box size scales as  $L \propto N_{\text{tot}}^{\frac{1}{3}}$ . For the dilute system (33 kg/m<sup>3</sup> in Fig. S17),  $D^{\text{self}}$  of CO<sub>2</sub> and H<sub>2</sub> are nearly independent of the system size, while for the denser system (389 kg/m<sup>3</sup> in Fig. S18),  $D^{\text{self}}$  of CO<sub>2</sub> and H<sub>2</sub> are linearly related to  $N_{\text{tot}}^{-\frac{1}{3}}$  with a non-zero slope, suggesting a strong system-size dependence of  $D^{\text{self}}$ .



Figure S17: Finite-size corrections for self-diffusion coefficients of (a)  $CO_2$  and (b)  $H_2$  in an equimolar mixture, obtained from MD simulations for various system sizes (N=120, 250, 500, 1000, and 2000 molecules) at 5 MPa and 423.15 K. The mixture density is ca. 33 kg/m<sup>3</sup>. The red symbols represent self-diffusion coefficients from MD simulations, while the blue symbols are the Yeh-Hummer<sup>7</sup> corrected self-diffusion coefficients (refer to Eq. 4 in the main text). The blue dashed line displays the mean value of the blue symbols. Self-diffusion coefficients are nearly independent of the system size.



Figure S18: Finite-size corrections for self-diffusion coefficients of (a)  $CO_2$  and (b)  $H_2$  in an equimolar mixture, obtained from MD simulations for various system sizes (N=120, 250, 500, 1000, and 2000 molecules) at 50 MPa and 323.15 K. The mixture density is ca. 389 kg/m<sup>3</sup>. The red symbols represent self-diffusion coefficients from MD simulations, while the blue symbols are the Yeh-Hummer<sup>7</sup> corrected self-diffusion coefficients (refer to Eq. 4 in the main text). The red dashed line is a linear fit to the red symbols, whereas the blue dashed line displays the mean value of the blue symbols. Self-diffusion coefficients are strongly dependent of the system size. See Fig. S17.



 $_{127}$  S4.3 Self-diffusion coefficients of CO<sub>2</sub> and H<sub>2</sub>

Figure S19: Self diffusivities of  $H_2$  and  $CO_2$ , represented on a linear vertical axis, as a function of the mole fraction of hydrogen, for various pressures. The symbols are colored according to the legend in subfigure (f).

#### $_{128}$ S4.4 Ratio of self-diffusion coefficients of CO<sub>2</sub> and H<sub>2</sub>

<sup>129</sup> To test the validity of the Stokes-Einstein<sup>10</sup> relation for mixtures of  $CO_2$  and  $H_2$ , assuming <sup>130</sup> perfect-stick boundary conditions<sup>10,11</sup>, we calculate the ratio,

$$\frac{D_{H_2}^{\text{self}}}{D_{CO_2}^{\text{self}}} = \frac{k_B T}{6\pi\eta R_{H_2}^{\text{eff}}} \cdot \frac{6\pi\eta R_{CO_2}^{\text{eff}}}{k_B T} = \frac{R_{CO_2}^{\text{eff}}}{R_{H_2}^{\text{eff}}} \approx 3.14,$$
 (S6)

where  $R_{CO_2}^{\text{eff}}$  represents the separation between the carbon and oxygen atoms within the CO<sub>2</sub> molecule (1.16 Å), while  $R_{H_2}^{\text{eff}}$  denotes half the distance between the two hydrogen atoms in H<sub>2</sub> (0.37 Å).



Figure S20: Ratio of self diffusion coefficients of  $H_2$  and  $CO_2$  as a function of the mole fraction of hydrogen, for various pressures. The dashed line represents the ratio of the Stokes-Einstein relation used to evaluate  $D^{\text{self}}$  of  $CO_2$  and  $H_2$ , see Eq. S6. The symbols are colored according to the legend in subfigure (a).



Figure S21: Comparing self-diffusion coefficients of  $CO_2$  (triangles) and  $H_2$  (squares) in  $CO_2$ -H<sub>2</sub> mixtures versus their values in pure fluids at the same temperature and pressure, considering different pressures, temperatures, and hydrogen mole fractions. The symbols are colored according to the legend in subfigure (e). See Fig. S20.



Figure S22: Comparison of self-diffusivities of  $CO_2$  (triangles) and  $H_2$  (squares) in  $CO_2$ - $H_2$  mixtures with their values in pure fluids at the same temperature and pressure, for different pressures, temperatures, and mole fractions of hydrogen. Subfigures (b)-(f) are identical to Figs. S21(a)-(e), except that the data are plotted on a vertical axis that is scaled linearly. The symbols are colored according to the legend in subfigure (f). See also Fig. S20.

<sup>137</sup> S4.6 Effect of temperature on the self-diffusion coefficients of CO<sub>2</sub>

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#### and H<sub>2</sub> in CO<sub>2</sub>-H<sub>2</sub> mixtures



Figure S23: Comparing self-diffusion coefficients of  $CO_2$  (triangles) and  $H_2$  (squares) in  $CO_2$ -H<sub>2</sub> mixtures versus their values at  $T_0 = 323.15$  K, considering different pressures, temperatures, and hydrogen mole fractions. The symbols are colored according to the legend in subfigure (a). See also Figs. S21 and S22.

S4.7 Self-diffusion coefficients of H<sub>2</sub> and CO<sub>2</sub> as a function of mix ture density



Figure S24: Finite system-size corrected self-diffusion coefficients of  $CO_2$  (triangles) and  $H_2$  (squares) as a function of the mixture densities at various mole fractions of  $H_2$ . The uncertainties in the computed self-diffusion coefficients are smaller than the symbol sizes. The symbols are colored according to the legend in subfigure (a).

S32



Figure S25: Finite system-size corrected self-diffusion coefficients of  $CO_2$  (triangles) and  $H_2$  (squares) as a function of the mixture densities, represented on linear horizontal and vertical axes. The uncertainties in the computed self-diffusion coefficients are smaller than the symbol sizes. The symbols are colored according to the legend in subfigure (a).

# <sup>141</sup> S5 Thermodynamic factors of diffusion for $H_2$ -CO<sub>2</sub> mix-<sup>142</sup> tures

To compute the thermodynamic factors of binary mixtures of CO<sub>2</sub> and H<sub>2</sub>, we obtain the Gibbs excess energy  $G(p, T, x_{H_2})$  from REFPROP<sup>3</sup>, in units of J/mol. Values of G are normalized by RT, where R is the universal gas constant, and we define  $Q = G(p, T, x_{H_2})/RT$ . A least-squares regression fitting procedure is used to fit Q to a suitable model, such as the one proposed by Margules<sup>12,13</sup>:

$$Q^{\text{Mar}} = x_{\text{H}_2} (1 - x_{\text{H}_2}) (A_{12} (1 - x_{\text{H}_2}) + A_{21} x_{\text{H}_2})$$
(S7)

where  $A_{12}$  and  $A_{21}$  are the fitting parameters. The value of  $\Gamma$  can be obtained by differentiating  $Q^{12}$ ,

$$\Gamma = 1 + 2x_{\rm H_2} \ (1 - x_{\rm H_2}) \ (\ (A_{21} - A_{12})(1 - 3x_{\rm H_2}) - A_{12}). \tag{S8}$$

<sup>143</sup> The van Laar model<sup>12</sup> is an alternative activity coefficient model<sup>12</sup>. We found that the <sup>144</sup> thermodynamic factors predicted by the Margules and van Laar models exhibit a variation <sup>145</sup> of less than 1% for all values of p, T, and  $x_{H_2}$ , suggesting that the values of  $\Gamma$  are minimally <sup>146</sup> affected by the underlying activity coefficient model.

# <sup>147</sup> S6 Maxwell-Stefan and Fick Diffusion coefficients of <sup>148</sup> H<sub>2</sub>-CO<sub>2</sub> mixtures

The MS diffusion coefficients are determined by first calculating the Onsager coefficients  $\Lambda_{ik}$ at zero total linear momentum<sup>14–16</sup>.  $\Lambda_{ik}$  is computed from the cross-correlations between the molecular displacements of species *i* and  $k^{4,14-16}$ ,

$$\Lambda_{ik} = \lim_{t \to \infty} \frac{\mathrm{d}}{\mathrm{dt}} \left[ \frac{1}{6N_{\mathrm{tot}}} \left\langle \left( \sum_{l=1}^{N_i} \left( \mathbf{r}_{l,i}(t) - \mathbf{r}_{l,i}(0) \right) \right) \times \left( \sum_{m=1}^{N_k} \left( \mathbf{r}_{m,k}(t) - \mathbf{r}_{m,k}(0) \right) \right) \right\rangle \right]$$
(S9)

where  $N_{\text{tot}}$  is the total number of molecules in a binary system consisting of  $N_i$  and  $N_k$ molecules of type *i* and *k*, respectively. Similar to the calculation of  $\eta$  and  $D^{\text{self}}$ , the segment of the cross-correlations with a slope between 0.99 and 1.01 on a log-log plot is chosen for the calculation of the Onsager coefficients, also see Fig. S26 of the Supporting Information. The MS diffusion coefficient  $D^{\text{MS,MD}}$  for a binary mixture is then expressed as a linear combination of the Onsager coefficients<sup>4,14–16</sup>,

<sup>159</sup> 
$$D^{\text{MS,MD}} = \frac{x_2}{x_1} \Lambda_{11} + \frac{x_1}{x_2} \Lambda_{22} - 2\Lambda_{12}$$
 (S10)

where  $x_1$  and  $x_2$  are the mole fractions of the components in the binary mixture.

Determination of Maxwell-Stefan diffusion coefficient from S6.1 161 MD simulations 162



Figure S26: (a) Cross correlations of molecular displacements (Eq. S9 in the main text)  $(MSD_{Onsg})$  are examined as a function of time in an equimolar mixture of H<sub>2</sub> and CO<sub>2</sub> at 323.15 K and 50 MPa. These correlations can have positive values for like species interactions (e.g., Carbon-Carbon in  $CO_2$  shown in red symbols) and negative values for unlike species interactions (e.g., Carbon-Hydrogen shown in blue symbols). (b) Onsager coefficients (as per Eq. 9 in the main text) are derived by first plotting the absolute values of the cross correlations on a log-log scale and identifying the region with a slope within 1% of unity, see also Figs. S11 and S16. The sign of the slopes are adjusted based on the displacements shown in (a), are used for evaluation of the Maxwell-Stefan diffusion coefficient using Eq. 9 of the main text.
## <sup>163</sup> S6.2 Finite system-size effects at $\rho$ =389 kg/m<sup>3</sup>

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 $\left(\frac{1}{2000}\right)^{\frac{1}{3}}\left(\frac{1}{1000}\right)^{\frac{1}{3}}$ 

 $\left(\frac{1}{500}\right)^{\frac{1}{3}}$ 

 $1/N^{1/3}$ 

 $\left(\frac{1}{250}\right)^{\frac{1}{3}}$ 

<sup>164</sup> Jamali *et al.*<sup>17</sup> showed that the MS diffusion coefficients can be corrected according to,

$$D^{\rm MS} = D^{\rm MS, \rm MD} + \frac{1}{\Gamma} D^{\rm YH}$$
(S11)

where  $D^{\text{MS}}$  is the finite size corrected MS diffusivity,  $D^{\text{YH}}$  is the correction proposed by Yeh and Hummer<sup>7</sup> for correcting self-diffusion coefficients computed from finite-size systems (see Eq. S5) and  $\Gamma$  is the thermodynamic factor. In the same article, Jamali *et al.*<sup>17</sup> suggested that one only needs the Yeh-Hummer correction term<sup>7</sup>  $D^{\text{YH}}$  to obtain the Fick diffusion coefficients in the thermodynamic limit<sup>12,17</sup>,



 $\left(\frac{1}{2000}\right)^{\frac{1}{3}}\left(\frac{1}{1000}\right)^{\frac{1}{3}}$ 

 $\left(\frac{1}{120}\right)^{-1}$ 

 $\left(\frac{1}{250}\right)^{\frac{1}{3}}$ 

 $\left(\frac{1}{500}\right)^{\frac{1}{3}}$ 

 $1/N^{1/3}$ 

Figure S27: Illustration of finite-size effects in the calculation of Maxwell-Stefan and Fick diffusion coefficients for an equimolar mixture at 50 MPa and 323.15 K ( $\rho \approx 389 \text{ kg/m}^3$ ). The thermodynamic factor  $\Gamma$  used for the correction of the Maxwell-Stefan (see Eq. S11) and Fick diffusion coefficients (see Eq. S12) equals 0.31.

 $\left(\frac{1}{120}\right)^{\frac{1}{3}}$ 



 $_{172}$  S6.3 Fick diffusion coefficients of H<sub>2</sub>-CO<sub>2</sub> mixtures

Figure S28: Finite-system-size-corrected Fick diffusion coefficients as a function of the mole fraction of hydrogen  $(x_{\rm H_2})$ . Lines are colored as per the legend in subfigure (b). The dashed lines act as guides to the eye.

173 S6.4 Effect of  $H_2$  mole fraction on the Fick diffusion coefficients

## 174

## of H<sub>2</sub>-CO<sub>2</sub> mixtures



Figure S29: Ratio of the Fick diffusion coefficients, computed from MD simulations, at a given pressure and temperature with respect to the corresponding value at a reference hydrogen mole fraction  $x_{\rm H_2}^0 = 0.1$ .

175 S6.5 Effect of temperature on the Fick diffusion coefficients of  $H_2$ -CO<sub>2</sub> mixtures



Figure S30: The ratio of Fick diffusion coefficients at a particular mole fraction of  $H_2$  and temperature compared to their values at  $T_0 = 323.15$  K.



Figure S31: Principle of corresponding states applied to the product of the computed Fick diffusivity and the corresponding mixture density. Here, the reference density  $\rho_0$  for a mixture is calculated at 0.1 MPa and 298.15 K using the ideal-gas equation of state. The black dashed line at unity is plotted to identify the corresponding states.

## $_{177}$ S7 Phase equilibria of CO<sub>2</sub>-NaCl brine systems



#### $_{178}$ S7.1 Effect of pressure on the solubility of CO<sub>2</sub>

Figure S32: CO<sub>2</sub> solubilities, computed from MC simulations, in NaCl brine compared to the corresponding solubility at 5 MPa  $(x_{CO_2}^{p^0})$ , at (a) 323.15 K and (b) 423.15 K.

### <sup>179</sup> S7.2 Effect of temperature on the solubility of $CO_2$



Figure S33: CO<sub>2</sub> solubilities, computed from MC simulations, in NaCl brine at  $T_1 = 423.15$  K compared to the corresponding solubility at  $T_0 = 323.15$  K. The dashed line is an indicator to identify the regime in which the solubility does not depend on the temperature.

 $_{180}$  S7.3 Effect of NaCl concentration on the solubility of CO<sub>2</sub>



Figure S34: CO<sub>2</sub> solubilities, computed from MC simulations, in NaCl brine compared to the corresponding solubilities in pure H<sub>2</sub>O ( $x_{CO_2}^{c_0}$ ), at (a) 323.15 K and (b) 423.15 K. Subfigures (c) and (d) depict the natural logarithm of the ratio between the solubilities of CO<sub>2</sub> and its solubility in pure water at the same pressure and temperature computed from MC simulations, plotted as a function of the NaCl concentration in brine. Linear fits to the data points, indicated by dashed lines, reveal consistent slopes of ca. -0.23 and ca -0.21 for all lines in subfigures (c) and (d), respectively.

## $_{181}$ S8 Phase equilibria of H<sub>2</sub>-NaCl brine systems

#### $_{182}$ S8.1 Effect of pressure on the solubility of H<sub>2</sub>



Figure S35: H<sub>2</sub> solubilities, computed from MC simulations, in NaCl brine compared to the corresponding solubility at 5 MPa  $(x_{H_2}^{p^0})$ , at (a) 323.15 K and (b) 423.15 K.

#### 183 S8.2 Effect of temperature on the solubility of $H_2$



Figure S36: H<sub>2</sub> solubilities, computed from MC simulations, in NaCl brine at  $T_1 = 423.15$  K compared to the corresponding solubilities at  $T_0 = 323.15$  K.

 $_{184}$  S8.3 Effect of NaCl concentration on the solubility of H<sub>2</sub>



Figure S37: H<sub>2</sub> solubilities, computed from MC simulations, in NaCl brine compared to the corresponding solubilities in pure H<sub>2</sub>O  $(x_{H_2}^0)$ , at (a) 323.15 K and (b) 423.15 K. Subfigures (c) and (d) depict the natural logarithm of the ratio between the solubilities of CO<sub>2</sub> and its solubility in pure water at the same pressure and temperature computed from MC simulations, plotted as a function of the NaCl concentration in brine. Linear fits to the data points, indicated by dashed lines, reveal slopes between -0.11 and -0.16 in subfigure (c) and slopes between -0.11 and -0.19 subfigure (d).

# <sup>185</sup> S9 Force field parameters

Table S1: Interaction parameters of the TraPPE force field of carbon dioxide  $O=C=O^{18}$ , and the three-site Marx force field for hydrogen<sup>19–21</sup>. Each row contains the LJ and the electrostatic interaction parameters for the atom highlighted between brackets []. Parameters between different species are calculated using the Lorentz-Berthelot mixing rules<sup>5,6</sup>, except between Na<sup>+</sup> and Cl<sup>-</sup> ions<sup>22,23</sup>, Na<sup>+</sup> ions and the oxygen atom in water (Ow), and Cl<sup>-</sup> ions and oxygen atoms in water (Ow)<sup>22,23</sup>.

Atom	$\varepsilon/k_B / [K]$	$\sigma$ / [Å]	$q \neq [e]$
O=[C]=O	27.0	2.80	0.70
[O]=C=O	79.0	3.05	-0.35
H-[L]-H	36.7	2.958	-0.936
[H]-L-H	-	-	0.468
М-[О]-Н	79.86	3.1589	0
М-О-[H]	-	-	0.53136
[M] H- O -H	-	-	-1.06272
[Na <sup>+</sup> ]Cl <sup>-</sup>	177.0848	2.21737	0.85
Na <sup>+</sup> [Cl <sup>-</sup> ]	9.251769	4.69906	-0.85
[Na <sup>+</sup> ][Cl <sup>-</sup> ]	173.06027	3.00512	-
[Na <sup>+</sup> ][Ow]	95.423247	2.60738	-
[Cl <sup>-</sup> ][Ow]	7.4548886	4.23867	-

# 186 S10 Raw simulation data

# S10.1 Densities, compressibilities and total energies from MD simulations ulations

Table S2: Densities ( $\rho$ ) and compressibilities (Z) obtained from MD simulations of CO<sub>2</sub>-H<sub>2</sub> mixtures comprising 2000 molecules are presented as functions of pressure, temperature, and mole fraction of H<sub>2</sub>. The average box length L of the cubic simulation box is reported in units of angstrom (Å). Densities and compressibilities from the REFPROP database<sup>3</sup> are included for comparison. Total energies ( $E_{tot}$ ) calculated for the systems in the NVE ensemble are also included.

p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
5	323.15	0.0	$112.66 \pm 0.13$	$102.22 \pm 0.34$	104.84	0.80	0.78	5.38	
5	323.15	0.1	$114.94 \pm 0.06$	$87.06 \pm 0.14$	89.25	0.85	0.81	5.65	
5	323.15	0.2	$116.75 \pm 0.02$	$74.31\pm0.03$	75.97	0.89	0.83	5.87	
5	323.15	0.3	$118.08 \pm 0.04$	$63.37\pm0.06$	64.37	0.92	0.85	6.06	
5	323.15	0.4	$119.21 \pm 0.06$	$53.35 \pm 0.08$	53.98	0.95	0.87	6.21	
5	323.15	0.5	$120.14 \pm 0.04$	$44.08 \pm 0.04$	44.47	0.97	0.89	6.34	
5	323.15	0.6	$120.88 \pm 0.02$	$35.38 \pm 0.02$	35.61	0.99	0.91	6.44	
5	323.15	0.7	$121.54 \pm 0.05$	$27.03 \pm 0.03$	27.21	1.01	0.92	6.52	
5	323.15	0.8	$121.85 \pm 0.04$	$19.12 \pm 0.02$	19.14	1.01	0.94	6.59	
5	323.15	0.9	$122.20 \pm 0.07$	$11.31 \pm 0.02$	11.32	1.02	0.95	6.65	
5	323.15	1.0	$122.34 \pm 0.01$	$3.66\pm0.01$	3.65	1.03	0.96	6.68	
5	348.15	0.0	$118.11 \pm 0.02$	$88.71 \pm 0.04$	90.46	0.86	0.97	6.13	
5	348.15	0.1	$119.67 \pm 0.04$	$77.14 \pm 0.09$	78.68	0.89	0.98	6.35	
5	348.15	0.2	$120.98 \pm 0.06$	$66.80 \pm 0.11$	67.99	0.92	0.99	6.52	
	Continued on next page								

p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]
5	348.15	0.3	$121.97 \pm 0.02$	$57.49 \pm 0.03$	58.23	0.94	1.00	6.67
5	348.15	0.4	$122.89 \pm 0.01$	$48.70\pm0.01$	49.21	0.97	1.01	6.79
5	348.15	0.5	$123.60 \pm 0.05$	$40.47\pm0.05$	40.78	0.98	1.01	6.91
5	348.15	0.6	$124.27 \pm 0.03$	$32.56\pm0.02$	32.79	1.00	1.02	7.00
5	348.15	0.7	$124.73 \pm 0.02$	$25.01\pm0.01$	25.14	1.01	1.02	7.07
5	348.15	0.8	$125.04 \pm 0.03$	$17.69\pm0.02$	17.73	1.02	1.03	7.13
5	348.15	0.9	$125.22 \pm 0.04$	$10.51\pm0.01$	10.50	1.02	1.03	7.17
5	348.15	1.0	$125.40 \pm 0.03$	$3.40\pm0.01$	3.39	1.03	0.84	7.21
5	373.15	0.0	$122.54 \pm 0.03$	$79.44\pm0.05$	80.65	0.89	0.86	6.82
5	373.15	0.1	$123.74 \pm 0.06$	$69.78\pm0.11$	70.94	0.92	0.87	6.99
5	373.15	0.2	$124.74 \pm 0.04$	$60.94\pm0.06$	61.85	0.94	0.89	7.14
5	373.15	0.3	$125.61 \pm 0.09$	$52.64 \pm 0.12$	53.34	0.96	0.90	7.26
5	373.15	0.4	$126.28 \pm 0.01$	$44.88 \pm 0.01$	45.32	0.98	0.92	7.37
5	373.15	0.5	$126.84 \pm 0.03$	$37.46\pm0.03$	37.71	0.99	0.93	7.46
5	373.15	0.6	$127.36 \pm 0.07$	$30.25\pm0.05$	30.42	1.00	0.94	7.54
5	373.15	0.7	$127.74 \pm 0.01$	$23.29\pm0.01$	23.38	1.01	0.96	7.61
5	373.15	0.8	$128.05 \pm 0.02$	$16.47\pm0.01$	16.53	1.02	0.97	7.66
5	373.15	0.9	$128.18 \pm 0.03$	$9.80\pm0.01$	9.80	1.02	0.97	7.70
5	373.15	1.0	$128.26 \pm 0.04$	$3.17\pm0.01$	3.17	1.02	0.98	7.73
5	398.15	0.0	$126.45 \pm 0.01$	$72.29\pm0.01$	73.28	0.92	0.99	7.47
5	398.15	0.1	$127.33 \pm 0.03$	$64.04 \pm 0.05$	64.91	0.94	1.00	7.60
5	398.15	0.2	$128.17 \pm 0.05$	$56.17\pm0.07$	56.92	0.96	1.00	7.73
5	398.15	0.3	$128.81 \pm 0.03$	$48.81 \pm 0.03$	49.32	0.97	1.01	7.83
			Contin	ued on next pag	ge			

p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
5	398.15	0.4	$129.41 \pm 0.02$	$41.70 \pm 0.02$	42.07	0.99	1.01	7.93		
5	398.15	0.5	$129.88 \pm 0.08$	$34.88 \pm 0.06$	35.11	1.00	1.02	8.01		
5	398.15	0.6	$130.29 \pm 0.02$	$28.25 \pm 0.01$	28.39	1.01	1.02	8.08		
5	398.15	0.7	$130.61 \pm 0.02$	$21.78 \pm 0.01$	21.86	1.01	1.02	8.14		
5	398.15	0.8	$130.82 \pm 0.06$	$15.45 \pm 0.02$	15.47	1.02	1.03	8.19		
5	398.15	0.9	$130.96 \pm 0.01$	$9.19\pm0.01$	9.19	1.02	0.88	8.23		
5	398.15	1.0	$131.03 \pm 0.02$	$2.98\pm0.01$	2.97	1.02	0.89	8.25		
5	423.15	0.0	$129.83 \pm 0.02$	$66.79 \pm 0.03$	67.43	0.94	0.90	8.07		
5	423.15	0.1	$130.59 \pm 0.01$	$59.37 \pm 0.02$	60.00	0.95	0.92	8.20		
5	423.15	0.2	$131.33 \pm 0.05$	$52.21 \pm 0.06$	52.83	0.97	0.93	8.30		
5	423.15	0.3	$131.79 \pm 0.03$	$45.57 \pm 0.03$	45.93	0.98	0.94	8.40		
5	423.15	0.4	$132.31 \pm 0.02$	$39.02 \pm 0.02$	39.29	0.99	0.95	8.48		
5	423.15	0.5	$132.80 \pm 0.08$	$32.63 \pm 0.06$	32.87	1.00	0.96	8.56		
5	423.15	0.6	$133.08 \pm 0.03$	$26.51 \pm 0.02$	26.63	1.01	0.97	8.62		
5	423.15	0.7	$133.33 \pm 0.03$	$20.48 \pm 0.02$	20.54	1.01	0.98	8.67		
5	423.15	0.8	$133.48 \pm 0.03$	$14.54 \pm 0.01$	14.55	1.02	0.98	8.72		
5	423.15	0.9	$133.65 \pm 0.02$	$8.65\pm0.01$	8.65	1.02	0.99	8.75		
5	423.15	1.0	$133.68 \pm 0.01$	$2.80\pm0.01$	2.80	1.02	1.00	8.77		
10	323.15	0.0	$73.37 \pm 0.32$	$369.98 \pm 4.89$	384.33	0.44	1.00	2.23		
10	323.15	0.1	$84.18 \pm 0.05$	$221.63 \pm 0.43$	235.85	0.67	1.01	4.10		
10	323.15	0.2	$88.43 \pm 0.06$	$171.04 \pm 0.33$	178.75	0.77	1.01	4.82		
10	323.15	0.3	$91.20 \pm 0.02$	$137.51 \pm 0.09$	142.02	0.85	1.02	5.31		
10	323.15	0.4	$93.19 \pm 0.05$	$111.66 \pm 0.18$	114.31	0.91	1.02	5.66		
	Continued on next page									

p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
10	323.15	0.5	$94.67\pm0.01$	$90.09 \pm 0.04$	91.58	0.95	1.02	5.95	
10	323.15	0.6	$95.80\pm0.02$	$71.06 \pm 0.05$	71.87	0.99	1.02	6.17	
10	323.15	0.7	$96.64 \pm 0.02$	$53.78 \pm 0.04$	54.13	1.01	1.03	6.34	
10	323.15	0.8	$97.34 \pm 0.04$	$37.50 \pm 0.04$	37.69	1.03	0.91	6.48	
10	323.15	0.9	$97.74 \pm 0.01$	$22.11 \pm 0.01$	22.11	1.05	0.92	6.58	
10	323.15	1.0	$98.03 \pm 0.02$	$7.11\pm0.01$	7.10	1.06	0.93	6.65	
10	348.15	0.0	$86.71 \pm 0.18$	$224.16 \pm 1.40$	233.43	0.68	0.94	4.55	
10	348.15	0.1	$90.64 \pm 0.06$	$177.55 \pm 0.38$	185.28	0.77	0.95	5.24	
10	348.15	0.2	$93.20\pm0.08$	$146.10 \pm 0.37$	151.15	0.84	0.95	5.70	
10	348.15	0.3	$95.11 \pm 0.04$	$121.25 \pm 0.14$	124.46	0.90	0.96	6.06	
10	348.15	0.4	$96.61 \pm 0.03$	$100.22 \pm 0.10$	102.29	0.94	0.97	6.34	
10	348.15	0.5	$97.72 \pm 0.04$	$81.91 \pm 0.10$	83.05	0.97	0.98	6.57	
10	348.15	0.6	$98.61 \pm 0.04$	$65.16 \pm 0.08$	65.78	1.00	0.98	6.75	
10	348.15	0.7	$99.29\pm0.02$	$49.58 \pm 0.03$	49.86	1.02	0.99	6.90	
10	348.15	0.8	$99.81 \pm 0.04$	$34.78 \pm 0.04$	34.88	1.03	1.00	7.02	
10	348.15	0.9	$100.21 \pm 0.03$	$20.51 \pm 0.02$	20.53	1.05	1.00	7.11	
10	348.15	1.0	$100.39 \pm 0.03$	$6.62\pm0.01$	6.61	1.05	1.01	7.18	
10	373.15	0.0	$92.73 \pm 0.08$	$183.33 \pm 0.47$	188.57	0.77	1.01	5.65	
10	373.15	0.1	$95.29\pm0.07$	$152.81 \pm 0.33$	158.17	0.84	1.01	6.11	
10	373.15	0.2	$97.04 \pm 0.07$	$129.41 \pm 0.26$	133.09	0.89	1.02	6.45	
10	373.15	0.3	$98.44 \pm 0.07$	$109.35 \pm 0.24$	111.73	0.93	1.02	6.74	
10	373.15	0.4	$99.66 \pm 0.04$	$91.30 \pm 0.10$	93.02	0.96	1.02	6.97	
10	373.15	0.5	$100.56 \pm 0.02$	$75.16 \pm 0.05$	76.20	0.99	1.02	7.17	
	Continued on next page								

p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m	$n^3$ ]		Ζ	$E_{\rm tot}$
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]
10	373.15	0.6	$101.30 \pm 0.03$	$60.10 \pm 0.05$	60.74	1.01	1.02	7.33
10	373.15	0.7	$101.85 \pm 0.02$	$45.94 \pm 0.03$	46.26	1.03	0.93	7.46
10	373.15	0.8	$102.27 \pm 0.04$	$32.34 \pm 0.04$	32.48	1.04	0.94	7.57
10	373.15	0.9	$102.53 \pm 0.03$	$19.15 \pm 0.02$	19.17	1.05	0.94	7.65
10	373.15	1.0	$102.64 \pm 0.02$	$6.19\pm0.01$	6.18	1.05	0.95	7.70
10	398.15	0.0	$97.09\pm0.05$	$159.68 \pm 0.23$	163.03	0.83	0.96	6.51
10	398.15	0.1	$98.95\pm0.04$	$136.47 \pm 0.14$	140.13	0.88	0.97	6.86
10	398.15	0.2	$100.29 \pm 0.04$	$117.23 \pm 0.16$	119.91	0.92	0.97	7.14
10	398.15	0.3	$101.53 \pm 0.05$	$99.68 \pm 0.14$	101.88	0.95	0.98	7.39
10	398.15	0.4	$102.40 \pm 0.03$	$84.17\pm0.07$	85.56	0.98	0.98	7.59
10	398.15	0.5	$103.14 \pm 0.01$	$69.66 \pm 0.02$	70.54	1.00	0.99	7.75
10	398.15	0.6	$103.69 \pm 0.02$	$56.05 \pm 0.04$	56.50	1.01	0.99	7.89
10	398.15	0.7	$104.17 \pm 0.02$	$42.94 \pm 0.03$	43.19	1.03	1.00	8.01
10	398.15	0.8	$104.47 \pm 0.04$	$30.33 \pm 0.04$	30.40	1.04	1.00	8.10
10	398.15	0.9	$104.78 \pm 0.02$	$17.95 \pm 0.01$	17.99	1.05	1.01	8.18
10	398.15	1.0	$104.80 \pm 0.03$	$5.82\pm0.01$	5.81	1.05	1.01	8.23
10	423.15	0.0	$100.76 \pm 0.02$	$142.88 \pm 0.07$	145.56	0.88	1.01	7.26
10	423.15	0.1	$102.18 \pm 0.04$	$123.95 \pm 0.14$	126.84	0.91	1.02	7.55
10	423.15	0.2	$103.19 \pm 0.07$	$107.64 \pm 0.22$	109.69	0.94	1.02	7.79
10	423.15	0.3	$104.17 \pm 0.05$	$92.29 \pm 0.13$	93.95	0.97	1.02	8.00
10	423.15	0.4	$104.93 \pm 0.05$	$78.22 \pm 0.12$	79.38	0.99	1.02	8.17
10	423.15	0.5	$105.52 \pm 0.01$	$65.05 \pm 0.03$	65.76	1.01	1.02	8.32
10	423.15	0.6	$106.03 \pm 0.02$	$52.42 \pm 0.03$	52.86	1.02	0.75	8.45
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p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m	$n^3$ ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
10	423.15	0.7	$106.40 \pm 0.03$	$40.30 \pm 0.03$	40.52	1.03	0.78	8.55	
10	423.15	0.8	$106.66 \pm 0.02$	$28.51 \pm 0.02$	28.59	1.04	0.81	8.64	
10	423.15	0.9	$106.87 \pm 0.02$	$16.91 \pm 0.01$	16.94	1.04	0.84	8.70	
10	423.15	1.0	$106.88 \pm 0.01$	$5.48 \pm 0.01$	5.48	1.04	0.86	8.75	
15	323.15	0.0	$59.13 \pm 0.04$	$707.13 \pm 1.36$	699.76	0.35	0.88	-1.16	
15	323.15	0.1	$67.13 \pm 0.05$	$437.04 \pm 0.97$	456.58	0.51	0.90	1.91	
15	323.15	0.2	$73.93 \pm 0.04$	$292.72 \pm 0.53$	309.70	0.68	0.92	3.61	
15	323.15	0.3	$77.88 \pm 0.04$	$220.86 \pm 0.37$	230.33	0.79	0.93	4.50	
15	323.15	0.4	$80.43 \pm 0.03$	$173.67 \pm 0.17$	178.43	0.87	0.95	5.12	
15	323.15	0.5	$82.35 \pm 0.03$	$136.85 \pm 0.17$	139.54	0.94	0.96	5.56	
15	323.15	0.6	$83.81 \pm 0.02$	$106.15 \pm 0.09$	107.77	0.99	0.97	5.90	
15	323.15	0.7	$84.79 \pm 0.01$	$79.61 \pm 0.04$	80.26	1.02	0.98	6.17	
15	323.15	0.8	$85.55 \pm 0.02$	$55.25 \pm 0.03$	55.45	1.05	0.99	6.37	
15	323.15	0.9	$86.01 \pm 0.01$	$32.45 \pm 0.01$	32.37	1.07	1.00	6.51	
15	323.15	1.0	$86.36 \pm 0.03$	$10.40 \pm 0.01$	10.36	1.08	1.01	6.62	
15	348.15	0.0	$68.65 \pm 0.02$	$451.71 \pm 0.47$	463.34	0.50	1.01	2.16	
15	348.15	0.1	$75.39 \pm 0.08$	$308.56 \pm 1.02$	325.46	0.67	1.02	3.88	
15	348.15	0.2	$79.30 \pm 0.06$	$237.18 \pm 0.52$	248.25	0.78	1.02	4.80	
15	348.15	0.3	$81.94 \pm 0.04$	$189.59 \pm 0.29$	196.44	0.86	1.03	5.43	
15	348.15	0.4	$83.86 \pm 0.03$	$153.22 \pm 0.14$	157.36	0.92	1.03	5.89	
15	348.15	0.5	$85.29 \pm 0.03$	$123.18 \pm 0.12$	125.55	0.97	0.82	6.24	
15	348.15	0.6	$86.40 \pm 0.02$	$96.86 \pm 0.06$	98.22	1.01	0.84	6.53	
15	348.15	0.7	$87.24 \pm 0.05$	$73.10 \pm 0.12$	73.80	1.04	0.86	6.75	
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
15	348.15	0.8	$87.80 \pm 0.02$	$51.11 \pm 0.04$	51.30	1.06	0.88	6.93	
15	348.15	0.9	$88.20\pm0.01$	$30.09 \pm 0.01$	30.08	1.07	0.90	7.06	
15	348.15	1.0	$88.42 \pm 0.01$	$9.69\pm0.01$	9.66	1.08	0.91	7.15	
15	373.15	0.0	$76.99\pm0.08$	$320.29 \pm 1.04$	332.35	0.66	0.93	4.19	
15	373.15	0.1	$80.78\pm0.02$	$250.81 \pm 0.15$	261.96	0.77	0.94	5.11	
15	373.15	0.2	$83.41 \pm 0.05$	$203.82 \pm 0.40$	211.96	0.84	0.95	5.74	
15	373.15	0.3	$85.29\pm0.07$	$168.14 \pm 0.44$	173.34	0.90	0.96	6.22	
15	373.15	0.4	$86.74 \pm 0.03$	$138.50 \pm 0.13$	141.69	0.95	0.97	6.58	
15	373.15	0.5	$87.88\pm0.06$	$112.60 \pm 0.22$	114.56	0.99	0.98	6.88	
15	373.15	0.6	$88.73 \pm 0.04$	$89.44 \pm 0.11$	90.44	1.02	0.99	7.13	
15	373.15	0.7	$89.44 \pm 0.02$	$67.83 \pm 0.05$	68.40	1.04	1.00	7.32	
15	373.15	0.8	$89.91 \pm 0.03$	$47.59 \pm 0.05$	47.78	1.06	1.00	7.48	
15	373.15	0.9	$90.23\pm0.03$	$28.10 \pm 0.03$	28.11	1.07	1.01	7.60	
15	373.15	1.0	$90.37\pm0.01$	$9.07\pm0.01$	9.05	1.07	1.02	7.68	
15	398.15	0.0	$82.26 \pm 0.11$	$262.54 \pm 1.10$	270.74	0.76	1.02	5.43	
15	398.15	0.1	$84.87\pm0.03$	$216.27 \pm 0.24$	224.58	0.83	1.02	6.06	
15	398.15	0.2	$86.74 \pm 0.02$	$181.23 \pm 0.11$	187.35	0.89	1.03	6.55	
15	398.15	0.3	$88.13 \pm 0.04$	$152.40 \pm 0.21$	156.25	0.93	1.03	6.93	
15	398.15	0.4	$89.35 \pm 0.02$	$126.69 \pm 0.07$	129.43	0.97	0.87	7.25	
15	398.15	0.5	$90.26 \pm 0.06$	$103.92 \pm 0.21$	105.62	1.00	0.88	7.50	
15	398.15	0.6	$90.98\pm0.02$	$82.96 \pm 0.06$	83.95	1.03	0.89	7.71	
15	398.15	0.7	$91.51\pm0.02$	$63.34 \pm 0.03$	63.80	1.05	0.91	7.88	
15	398.15	0.8	$91.90\pm0.01$	$44.56 \pm 0.01$	44.73	1.06	0.92	8.02	
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
15	398.15	0.9	$92.14 \pm 0.02$	$26.39 \pm 0.02$	26.39	1.07	0.93	8.13	
15	398.15	1.0	$92.24\pm0.04$	$8.53\pm0.01$	8.52	1.07	0.94	8.21	
15	423.15	0.0	$86.28\pm0.04$	$227.57 \pm 0.29$	233.93	0.82	0.95	6.39	
15	423.15	0.1	$88.10 \pm 0.03$	$193.34 \pm 0.18$	199.18	0.88	0.96	6.88	
15	423.15	0.2	$89.55 \pm 0.03$	$164.68 \pm 0.18$	169.18	0.92	0.97	7.27	
15	423.15	0.3	$90.73\pm0.02$	$139.66 \pm 0.09$	142.91	0.96	0.98	7.60	
15	423.15	0.4	$91.66\pm0.02$	$117.36 \pm 0.08$	119.47	0.99	0.99	7.87	
15	423.15	0.5	$92.41 \pm 0.02$	$96.85 \pm 0.06$	98.16	1.01	1.00	8.10	
15	423.15	0.6	$93.03\pm0.02$	$77.60 \pm 0.04$	78.42	1.03	1.00	8.28	
15	423.15	0.7	$93.47\pm0.01$	$59.44 \pm 0.02$	59.83	1.05	1.01	8.44	
15	423.15	0.8	$93.81\pm0.03$	$41.89 \pm 0.04$	42.07	1.06	1.01	8.57	
15	423.15	0.9	$93.98\pm0.02$	$24.87 \pm 0.01$	24.88	1.07	1.02	8.66	
15	423.15	1.0	$94.07\pm0.01$	$8.04 \pm 0.01$	8.04	1.07	1.02	8.73	
20	323.15	0.0	$57.20 \pm 0.02$	$781.16 \pm 0.72$	784.30	0.42	1.02	-1.94	
20	323.15	0.1	$60.90\pm0.04$	$585.22 \pm 1.09$	589.51	0.51	1.03	0.51	
20	323.15	0.2	$65.84 \pm 0.02$	$414.30 \pm 0.41$	427.97	0.64	1.03	2.46	
20	323.15	0.3	$69.88 \pm 0.02$	$305.73 \pm 0.23$	316.48	0.76	0.90	3.73	
20	323.15	0.4	$72.72 \pm 0.06$	$235.05 \pm 0.61$	241.10	0.86	0.91	4.58	
20	323.15	0.5	$74.80\pm0.02$	$182.64 \pm 0.13$	185.99	0.94	0.92	5.19	
20	323.15	0.6	$76.31\pm0.02$	$140.62 \pm 0.12$	142.21	1.00	0.93	5.65	
20	323.15	0.7	$77.49 \pm 0.02$	$104.32 \pm 0.09$	105.17	1.04	0.94	6.00	
20	323.15	0.8	$78.31\pm0.01$	$72.02 \pm 0.03$	72.30	1.08	0.95	6.26	
20	323.15	0.9	$78.83\pm0.02$	$42.14 \pm 0.03$	42.06	1.10	0.96	6.46	
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]
20	323.15	1.0	$79.10\pm0.03$	$13.53 \pm 0.02$	13.45	1.11	0.97	6.59
20	348.15	0.0	$61.75 \pm 0.08$	$620.72 \pm 2.37$	626.22	0.49	0.98	0.47
20	348.15	0.1	$66.82\pm0.07$	$443.10 \pm 1.43$	459.29	0.62	0.98	2.58
20	348.15	0.2	$70.92\pm0.07$	$331.49 \pm 0.98$	345.44	0.74	0.99	3.92
20	348.15	0.3	$73.88 \pm 0.10$	$258.72 \pm 1.05$	268.02	0.84	1.00	4.81
20	348.15	0.4	$75.99\pm0.02$	$205.96 \pm 0.18$	211.39	0.91	1.00	5.45
20	348.15	0.5	$77.58\pm0.03$	$163.66 \pm 0.17$	166.77	0.97	1.01	5.92
20	348.15	0.6	$78.77\pm0.01$	$127.83 \pm 0.03$	129.41	1.02	1.01	6.31
20	348.15	0.7	$79.67\pm0.01$	$95.96 \pm 0.01$	96.68	1.05	1.01	6.60
20	348.15	0.8	$80.35 \pm 0.01$	$66.67 \pm 0.02$	66.93	1.08	1.02	6.83
20	348.15	0.9	$80.78 \pm 0.03$	$39.16 \pm 0.05$	39.14	1.10	1.02	7.01
20	348.15	1.0	$81.00 \pm 0.03$	$12.60 \pm 0.01$	12.56	1.11	1.02	7.12
20	373.15	0.0	$67.85 \pm 0.06$	$467.88 \pm 1.15$	480.55	0.61	1.03	2.71
20	373.15	0.1	$71.97\pm0.05$	$354.59 \pm 0.67$	369.17	0.72	1.03	4.11
20	373.15	0.2	$74.91\pm0.01$	$281.37 \pm 0.12$	291.90	0.82	0.92	5.02
20	373.15	0.3	$77.14 \pm 0.04$	$227.24 \pm 0.35$	234.64	0.89	0.93	5.70
20	373.15	0.4	$78.77\pm0.03$	$184.91 \pm 0.25$	189.41	0.95	0.94	6.20
20	373.15	0.5	$80.01 \pm 0.02$	$149.24 \pm 0.11$	151.76	0.99	0.95	6.61
20	373.15	0.6	$81.01 \pm 0.02$	$117.54 \pm 0.08$	119.02	1.03	0.95	6.93
20	373.15	0.7	$81.74 \pm 0.05$	$88.88 \pm 0.16$	89.59	1.06	0.96	7.19
20	373.15	0.8	$82.27\pm0.02$	$62.12 \pm 0.03$	62.37	1.08	0.97	7.40
20	373.15	0.9	$82.62 \pm 0.02$	$36.60 \pm 0.03$	36.62	1.09	0.98	7.55
20	373.15	1.0	$82.77\pm0.02$	$11.81 \pm 0.01$	11.79	1.10	0.98	7.66
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
20	398.15	0.0	$73.04 \pm 0.01$	$375.14 \pm 0.15$	385.81	0.71	0.99	4.29	
20	398.15	0.1	$76.04\pm0.01$	$300.72 \pm 0.08$	311.92	0.80	0.99	5.26	
20	398.15	0.2	$78.29\pm0.07$	$246.42 \pm 0.66$	255.41	0.87	1.00	5.96	
20	398.15	0.3	$79.97\pm0.02$	$203.99 \pm 0.18$	210.16	0.93	1.00	6.48	
20	398.15	0.4	$81.25\pm0.01$	$168.46 \pm 0.07$	172.36	0.98	1.01	6.91	
20	398.15	0.5	$82.26\pm0.02$	$137.28 \pm 0.11$	139.63	1.01	1.01	7.26	
20	398.15	0.6	$83.06 \pm 0.03$	$109.03 \pm 0.13$	110.38	1.04	1.02	7.54	
20	398.15	0.7	$83.63\pm0.02$	$82.97\pm0.07$	83.56	1.06	1.02	7.77	
20	398.15	0.8	$84.08 \pm 0.02$	$58.20 \pm 0.05$	58.42	1.08	1.02	7.95	
20	398.15	0.9	$84.33 \pm 0.01$	$34.42 \pm 0.01$	34.42	1.09	1.02	8.08	
20	398.15	1.0	$84.43 \pm 0.03$	$11.12 \pm 0.01$	11.11	1.09	1.02	8.19	
20	423.15	0.0	$77.21 \pm 0.02$	$317.52 \pm 0.20$	327.10	0.79	1.02	5.49	
20	423.15	0.1	$79.40\pm0.01$	$264.10 \pm 0.12$	273.25	0.86	0.73	6.21	
20	423.15	0.2	$81.07\pm0.03$	$221.98 \pm 0.27$	228.84	0.91	0.76	6.76	
20	423.15	0.3	$82.44 \pm 0.03$	$186.20 \pm 0.23$	191.27	0.96	0.79	7.21	
20	423.15	0.4	$83.48 \pm 0.04$	$155.35 \pm 0.21$	158.64	1.00	0.82	7.58	
20	423.15	0.5	$84.32 \pm 0.04$	$127.48 \pm 0.18$	129.57	1.03	0.85	7.88	
20	423.15	0.6	$84.97\pm0.02$	$101.85 \pm 0.08$	103.05	1.05	0.87	8.13	
20	423.15	0.7	$85.43 \pm 0.02$	$77.85 \pm 0.07$	78.37	1.07	0.89	8.33	
20	423.15	0.8	$85.78 \pm 0.02$	$54.79 \pm 0.04$	54.98	1.08	0.91	8.49	
20	423.15	0.9	$85.99\pm0.03$	$32.47 \pm 0.03$	32.47	1.09	0.93	8.62	
20	423.15	1.0	$86.09 \pm 0.01$	$10.50 \pm 0.01$	10.50	1.09	0.94	8.72	
25	323.15	0.0	$56.08\pm0.03$	$828.89 \pm 1.24$	834.21	0.49	0.96	-2.45	
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	$n^3$ ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
25	323.15	0.1	$58.28 \pm 0.02$	$667.96 \pm 0.53$	660.61	0.55	0.97	-0.28	
25	323.15	0.2	$61.61\pm0.02$	$505.83 \pm 0.38$	508.88	0.66	0.98	1.64	
25	323.15	0.3	$64.90\pm0.04$	$381.66 \pm 0.64$	387.88	0.77	0.99	3.08	
25	323.15	0.4	$67.64\pm0.03$	$292.10 \pm 0.45$	297.32	0.87	1.00	4.10	
25	323.15	0.5	$69.69\pm0.01$	$225.83 \pm 0.14$	228.86	0.95	1.01	4.85	
25	323.15	0.6	$71.27\pm0.01$	$172.58 \pm 0.10$	174.38	1.01	1.02	5.42	
25	323.15	0.7	$72.43 \pm 0.02$	$127.74 \pm 0.10$	128.55	1.06	1.02	5.84	
25	323.15	0.8	$73.23\pm0.03$	$88.09 \pm 0.11$	88.16	1.10	1.03	6.16	
25	323.15	0.9	$73.80\pm0.02$	$51.36 \pm 0.04$	51.21	1.13	1.03	6.40	
25	323.15	1.0	$74.09\pm0.01$	$16.46 \pm 0.01$	16.38	1.14	1.03	6.56	
25	348.15	0.0	$59.24 \pm 0.02$	$703.21 \pm 0.67$	711.60	0.54	0.80	-0.37	
25	348.15	0.1	$62.44 \pm 0.02$	$543.13 \pm 0.46$	551.93	0.63	0.83	1.64	
25	348.15	0.2	$65.79 \pm 0.04$	$415.37 \pm 0.75$	426.44	0.74	0.85	3.16	
25	348.15	0.3	$68.49\pm0.03$	$324.69 \pm 0.41$	332.46	0.84	0.87	4.24	
25	348.15	0.4	$70.67\pm0.01$	$256.10 \pm 0.08$	261.47	0.92	0.89	5.03	
25	348.15	0.5	$72.27\pm0.02$	$202.45 \pm 0.18$	205.40	0.98	0.90	5.63	
25	348.15	0.6	$73.58\pm0.01$	$156.84 \pm 0.08$	158.79	1.04	0.92	6.11	
25	348.15	0.7	$74.50\pm0.01$	$117.40 \pm 0.05$	118.27	1.08	0.93	6.46	
25	348.15	0.8	$75.17\pm0.01$	$81.45 \pm 0.04$	81.71	1.10	0.95	6.74	
25	348.15	0.9	$75.61\pm0.02$	$47.76 \pm 0.04$	47.73	1.12	0.96	6.95	
25	348.15	1.0	$75.81\pm0.05$	$15.37 \pm 0.03$	15.32	1.13	0.97	7.10	
25	373.15	0.0	$63.31 \pm 0.03$	$576.06 \pm 0.79$	588.46	0.62	0.98	1.63	
25	373.15	0.1	$66.61 \pm 0.01$	$447.32 \pm 0.23$	460.40	0.72	0.99	3.23	
	Continued on next page								

p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
25	373.15	0.2	$69.46 \pm 0.02$	$352.87 \pm 0.26$	364.55	0.81	1.00	4.38		
25	373.15	0.3	$71.58\pm0.03$	$284.39 \pm 0.42$	291.79	0.89	1.01	5.21		
25	373.15	0.4	$73.30\pm0.04$	$229.43 \pm 0.33$	234.34	0.96	1.01	5.86		
25	373.15	0.5	$74.63\pm0.03$	$183.89 \pm 0.21$	186.93	1.01	1.02	6.36		
25	373.15	0.6	$75.62\pm0.03$	$144.48 \pm 0.18$	146.10	1.05	1.02	6.75		
25	373.15	0.7	$76.40\pm0.02$	$108.85 \pm 0.08$	109.68	1.08	1.03	7.07		
25	373.15	0.8	$76.93\pm0.01$	$75.95 \pm 0.02$	76.21	1.10	1.03	7.31		
25	373.15	0.9	$77.28\pm0.03$	$44.72 \pm 0.05$	44.71	1.12	1.03	7.50		
25	373.15	1.0	$77.41 \pm 0.02$	$14.43 \pm 0.01$	14.40	1.13	0.85	7.63		
25	398.15	0.0	$67.50 \pm 0.05$	$475.26 \pm 1.15$	487.81	0.70	0.87	3.30		
25	398.15	0.1	$70.37\pm0.03$	$379.36 \pm 0.50$	392.67	0.79	0.89	4.52		
25	398.15	0.2	$72.61\pm0.04$	$309.00 \pm 0.55$	319.46	0.87	0.90	5.40		
25	398.15	0.3	$74.28\pm0.04$	$254.49 \pm 0.36$	261.22	0.93	0.91	6.07		
25	398.15	0.4	$75.64\pm0.03$	$208.86 \pm 0.27$	213.13	0.98	0.93	6.59		
25	398.15	0.5	$76.70\pm0.02$	$169.41 \pm 0.15$	171.96	1.03	0.94	7.03		
25	398.15	0.6	$77.54\pm0.04$	$134.02 \pm 0.19$	135.52	1.06	0.95	7.38		
25	398.15	0.7	$78.14 \pm 0.02$	$101.72 \pm 0.08$	102.37	1.08	0.96	7.65		
25	398.15	0.8	$78.58\pm0.01$	$71.28 \pm 0.02$	71.46	1.10	0.97	7.88		
25	398.15	0.9	$78.89\pm0.02$	$42.05 \pm 0.03$	42.06	1.12	0.98	8.04		
25	398.15	1.0	$78.97\pm0.01$	$13.60 \pm 0.01$	13.58	1.12	0.99	8.17		
25	423.15	0.0	$71.25\pm0.06$	$404.06 \pm 1.05$	415.50	0.77	1.00	4.65		
25	423.15	0.1	$73.52 \pm 0.02$	$332.75 \pm 0.21$	343.87	0.85	1.00	5.57		
25	423.15	0.2	$75.27\pm0.02$	$277.35 \pm 0.19$	285.81	0.91	1.01	6.28		
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
25	423.15	0.3	$76.64\pm0.03$	$231.74 \pm 0.30$	237.46	0.96	1.01	6.84		
25	423.15	0.4	$77.77\pm0.02$	$192.11 \pm 0.16$	196.03	1.01	1.02	7.30		
25	423.15	0.5	$78.63\pm0.01$	$157.21 \pm 0.04$	159.54	1.04	1.02	7.67		
25	423.15	0.6	$79.32\pm0.01$	$125.21 \pm 0.07$	126.55	1.07	1.03	7.98		
25	423.15	0.7	$79.82\pm0.03$	$95.43 \pm 0.09$	96.05	1.09	1.03	8.23		
25	423.15	0.8	$80.18 \pm 0.02$	$67.10 \pm 0.05$	67.30	1.10	1.03	8.43		
25	423.15	0.9	$80.40 \pm 0.02$	$39.72 \pm 0.03$	39.73	1.11	0.89	8.58		
25	423.15	1.0	$80.46 \pm 0.02$	$12.85 \pm 0.01$	12.85	1.11	0.90	8.70		
30	323.15	0.0	$55.37\pm0.01$	$860.84 \pm 0.21$	870.43	0.57	0.91	-2.81		
30	323.15	0.1	$56.85 \pm 0.04$	$719.62 \pm 1.66$	707.86	0.62	0.92	-0.78		
30	323.15	0.2	$59.18 \pm 0.01$	$570.68 \pm 0.35$	564.61	0.70	0.93	1.08		
30	323.15	0.3	$61.73 \pm 0.03$	$443.56 \pm 0.55$	443.13	0.79	0.95	2.55		
30	323.15	0.4	$64.04\pm0.03$	$344.08 \pm 0.51$	345.05	0.88	0.96	3.69		
30	323.15	0.5	$66.00\pm0.01$	$265.79 \pm 0.15$	267.16	0.97	0.96	4.55		
30	323.15	0.6	$67.53 \pm 0.03$	$202.93 \pm 0.30$	203.82	1.04	0.97	5.20		
30	323.15	0.7	$68.67\pm0.02$	$149.90 \pm 0.16$	150.25	1.09	0.98	5.70		
30	323.15	0.8	$69.49\pm0.01$	$103.06 \pm 0.04$	103.01	1.13	0.99	6.07		
30	323.15	0.9	$70.04\pm0.01$	$60.06 \pm 0.03$	59.84	1.16	1.00	6.35		
30	323.15	1.0	$70.31\pm0.02$	$19.26 \pm 0.01$	19.15	1.17	1.00	6.54		
30	348.15	0.0	$57.79\pm0.01$	$757.25 \pm 0.23$	766.83	0.60	1.01	-0.95		
30	348.15	0.1	$59.96 \pm 0.03$	$613.18 \pm 1.05$	614.98	0.67	1.01	0.98		
30	348.15	0.2	$62.48 \pm 0.03$	$484.96 \pm 0.67$	488.55	0.76	1.02	2.54		
30	348.15	0.3	$64.86 \pm 0.04$	$382.34 \pm 0.62$	386.81	0.85	1.02	3.76		
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p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m <sup>3</sup> ]			Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
30	348.15	0.4	$66.88 \pm 0.04$	$302.13 \pm 0.51$	305.97	0.93	1.02	4.67	
30	348.15	0.5	$68.44 \pm 0.01$	$238.40 \pm 0.14$	240.69	1.00	1.03	5.37	
30	348.15	0.6	$69.66 \pm 0.01$	$184.83 \pm 0.04$	186.04	1.05	1.03	5.91	
30	348.15	0.7	$70.62\pm0.01$	$137.79 \pm 0.06$	138.49	1.10	1.03	6.34	
30	348.15	0.8	$71.26\pm0.02$	$95.58 \pm 0.08$	95.63	1.13	0.91	6.66	
30	348.15	0.9	$71.68\pm0.03$	$56.04 \pm 0.08$	55.85	1.15	0.92	6.91	
30	348.15	1.0	$71.90\pm0.01$	$18.01 \pm 0.01$	17.94	1.16	0.93	7.08	
30	373.15	0.0	$60.82\pm0.03$	$649.67 \pm 0.82$	661.87	0.66	0.94	0.88	
30	373.15	0.1	$63.29\pm0.05$	$521.50 \pm 1.20$	530.51	0.74	0.95	2.53	
30	373.15	0.2	$65.66 \pm 0.02$	$417.72 \pm 0.43$	425.73	0.82	0.96	3.80	
30	373.15	0.3	$67.73\pm0.05$	$335.74 \pm 0.74$	342.49	0.90	0.97	4.78	
30	373.15	0.4	$69.35 \pm 0.03$	$270.93 \pm 0.40$	275.36	0.97	0.97	5.53	
30	373.15	0.5	$70.62\pm0.02$	$217.02 \pm 0.17$	219.53	1.03	0.98	6.11	
30	373.15	0.6	$71.62\pm0.02$	$170.09 \pm 0.15$	171.44	1.07	0.99	6.58	
30	373.15	0.7	$72.39\pm0.02$	$127.94 \pm 0.11$	128.60	1.10	0.99	6.95	
30	373.15	0.8	$72.92\pm0.01$	$89.22 \pm 0.04$	89.32	1.13	1.00	7.24	
30	373.15	0.9	$73.26\pm0.01$	$52.49 \pm 0.01$	52.39	1.14	1.01	7.46	
30	373.15	1.0	$73.39\pm0.02$	$16.94 \pm 0.01$	16.88	1.15	1.01	7.62	
30	398.15	0.0	$64.16 \pm 0.05$	$553.42 \pm 1.35$	567.77	0.72	1.01	2.52	
30	398.15	0.1	$66.56 \pm 0.03$	$448.30 \pm 0.63$	461.20	0.80	1.02	3.87	
30	398.15	0.2	$68.54\pm0.01$	$367.35 \pm 0.19$	376.41	0.88	1.02	4.88	
30	398.15	0.3	$70.21\pm0.03$	$301.41 \pm 0.35$	307.85	0.94	1.02	5.68	
30	398.15	0.4	$71.53 \pm 0.02$	$246.88 \pm 0.19$	250.93	1.00	1.03	6.30	
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	$n^3$ ]		Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
30	398.15	0.5	$72.60\pm0.03$	$199.70 \pm 0.26$	202.22	1.04	1.03	6.81		
30	398.15	0.6	$73.43\pm0.03$	$157.79 \pm 0.17$	159.20	1.08	1.03	7.22		
30	398.15	0.7	$74.07\pm0.02$	$119.41 \pm 0.09$	120.16	1.11	0.70	7.54		
30	398.15	0.8	$74.50\pm0.02$	$83.66 \pm 0.06$	83.84	1.13	0.74	7.81		
30	398.15	0.9	$74.74\pm0.02$	$49.43 \pm 0.04$	49.35	1.14	0.77	8.01		
30	398.15	1.0	$74.87\pm0.01$	$15.96 \pm 0.01$	15.94	1.15	0.80	8.15		
30	423.15	0.0	$67.35 \pm 0.03$	$478.38 \pm 0.65$	491.99	0.78	0.83	3.92		
30	423.15	0.1	$69.38 \pm 0.01$	$395.89 \pm 0.14$	407.18	0.86	0.86	4.99		
30	423.15	0.2	$71.08\pm0.02$	$329.34 \pm 0.28$	338.00	0.92	0.88	5.83		
30	423.15	0.3	$72.43 \pm 0.02$	$274.51 \pm 0.24$	280.35	0.98	0.90	6.49		
30	423.15	0.4	$73.55 \pm 0.01$	$227.16 \pm 0.12$	231.05	1.02	0.92	7.03		
30	423.15	0.5	$74.44\pm0.01$	$185.26 \pm 0.05$	187.78	1.06	0.94	7.48		
30	423.15	0.6	$75.13 \pm 0.02$	$147.35 \pm 0.10$	148.79	1.09	0.95	7.84		
30	423.15	0.7	$75.65\pm0.01$	$112.10 \pm 0.06$	112.85	1.11	0.97	8.13		
30	423.15	0.8	$75.98\pm0.01$	$78.84 \pm 0.03$	79.04	1.13	0.98	8.37		
30	423.15	0.9	$76.19\pm0.04$	$46.68 \pm 0.07$	46.66	1.14	0.99	8.55		
30	423.15	1.0	$76.24\pm0.02$	$15.11 \pm 0.01$	15.11	1.14	1.00	8.68		
35	323.15	0.0	$54.79\pm0.02$	$888.51 \pm 0.80$	899.26	0.65	1.01	-3.12		
35	323.15	0.1	$55.89\pm0.01$	$757.42 \pm 0.56$	743.29	0.68	1.02	-1.16		
35	323.15	0.2	$57.57\pm0.02$	$619.71 \pm 0.67$	605.99	0.75	1.02	0.63		
35	323.15	0.3	$59.54 \pm 0.04$	$494.14 \pm 0.92$	486.19	0.83	1.03	2.13		
35	323.15	0.4	$61.51 \pm 0.02$	$388.28 \pm 0.35$	384.86	0.91	1.03	3.33		
35	323.15	0.5	$63.26\pm0.02$	$301.89 \pm 0.34$	300.73	0.99	1.04	4.28		
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p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m <sup>3</sup> ]			Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
35	323.15	0.6	$64.66 \pm 0.01$	$231.07 \pm 0.06$	230.50	1.06	0.79	5.00		
35	323.15	0.7	$65.77\pm0.01$	$170.57 \pm 0.08$	170.28	1.12	0.81	5.56		
35	323.15	0.8	$66.58\pm0.01$	$117.17 \pm 0.06$	116.88	1.16	0.83	5.99		
35	323.15	0.9	$67.09\pm0.01$	$68.36 \pm 0.05$	67.96	1.18	0.86	6.30		
35	323.15	1.0	$67.35 \pm 0.02$	$21.92 \pm 0.02$	21.78	1.20	0.88	6.52		
35	348.15	0.0	$56.85 \pm 0.01$	$795.33 \pm 0.39$	807.54	0.67	0.90	-1.35		
35	348.15	0.1	$58.41 \pm 0.02$	$663.50 \pm 0.77$	661.32	0.73	0.91	0.49		
35	348.15	0.2	$60.33 \pm 0.03$	$538.57 \pm 0.80$	536.41	0.80	0.93	2.07		
35	348.15	0.3	$62.34 \pm 0.02$	$430.57 \pm 0.49$	431.57	0.88	0.94	3.35		
35	348.15	0.4	$64.06 \pm 0.01$	$343.86 \pm 0.21$	344.69	0.96	0.96	4.33		
35	348.15	0.5	$65.54 \pm 0.01$	$271.50 \pm 0.04$	272.47	1.02	0.97	5.12		
35	348.15	0.6	$66.70\pm0.03$	$210.51 \pm 0.30$	211.08	1.08	0.98	5.73		
35	348.15	0.7	$67.60\pm0.03$	$157.09 \pm 0.18$	157.31	1.12	0.99	6.21		
35	348.15	0.8	$68.24\pm0.01$	$108.85 \pm 0.02$	108.71	1.16	1.00	6.59		
35	348.15	0.9	$68.66\pm0.01$	$63.77 \pm 0.02$	63.54	1.18	1.01	6.86		
35	348.15	1.0	$68.83\pm0.01$	$20.53 \pm 0.01$	20.44	1.19	1.01	7.06		
35	373.15	0.0	$59.27\pm0.03$	$701.93 \pm 0.89$	715.25	0.71	1.02	0.34		
35	373.15	0.1	$61.14 \pm 0.02$	$578.40 \pm 0.64$	584.25	0.78	1.02	1.99		
35	373.15	0.2	$63.09\pm0.01$	$470.85 \pm 0.14$	475.76	0.85	1.03	3.34		
35	373.15	0.3	$64.86 \pm 0.01$	$382.41 \pm 0.26$	386.27	0.93	1.03	4.39		
35	373.15	0.4	$66.34 \pm 0.02$	$309.47 \pm 0.22$	312.04	0.99	1.03	5.23		
35	373.15	0.5	$67.58 \pm 0.03$	$247.64 \pm 0.35$	249.37	1.05	0.84	5.89		
35	35       373.15       0.6       68.53 $\pm$ 0.01       194.10 $\pm$ 0.12       194.96       1.09       0.86       6.42									
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	$n^3$ ]		Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
35	373.15	0.7	$69.30 \pm 0.01$	$145.81 \pm 0.03$	146.34	1.13	0.88	6.84		
35	373.15	0.8	$69.81 \pm 0.02$	$101.69 \pm 0.11$	101.69	1.16	0.89	7.17		
35	373.15	0.9	$70.12\pm0.02$	$59.87 \pm 0.04$	59.68	1.17	0.91	7.42		
35	373.15	1.0	$70.24\pm0.03$	$19.32 \pm 0.02$	19.26	1.18	0.92	7.60		
35	398.15	0.0	$61.97\pm0.02$	$614.19 \pm 0.62$	629.17	0.76	0.94	1.92		
35	398.15	0.1	$63.89\pm0.03$	$506.98 \pm 0.64$	517.25	0.83	0.95	3.33		
35	398.15	0.2	$65.64\pm0.02$	$418.21 \pm 0.42$	425.44	0.90	0.96	4.44		
35	398.15	0.3	$67.17\pm0.02$	$344.23 \pm 0.34$	349.43	0.96	0.97	5.33		
35	398.15	0.4	$68.44 \pm 0.02$	$281.94 \pm 0.26$	285.43	1.02	0.98	6.04		
35	398.15	0.5	$69.43 \pm 0.02$	$228.32 \pm 0.18$	230.25	1.07	0.99	6.61		
35	398.15	0.6	$70.25\pm0.02$	$180.23 \pm 0.14$	181.36	1.10	1.00	7.07		
35	398.15	0.7	$70.85\pm0.01$	$136.48 \pm 0.06$	136.93	1.13	1.00	7.45		
35	398.15	0.8	$71.28\pm0.03$	$95.49 \pm 0.11$	95.58	1.15	1.01	7.75		
35	398.15	0.9	$71.54\pm0.02$	$56.38 \pm 0.06$	56.29	1.17	1.02	7.97		
35	398.15	1.0	$71.62\pm0.01$	$18.22 \pm 0.01$	18.21	1.17	1.02	8.13		
35	423.15	0.0	$64.66\pm0.04$	$540.61 \pm 0.94$	555.23	0.81	1.03	3.30		
35	423.15	0.1	$66.41 \pm 0.01$	$451.50 \pm 0.12$	461.84	0.88	1.03	4.48		
35	423.15	0.2	$68.00\pm0.05$	$376.18 \pm 0.75$	384.53	0.94	1.03	5.42		
35	423.15	0.3	$69.29\pm0.02$	$313.63 \pm 0.31$	319.40	1.00	1.03	6.18		
35	423.15	0.4	$70.31\pm0.01$	$260.04 \pm 0.10$	263.41	1.04	0.88	6.79		
35	423.15	0.5	$71.19\pm0.02$	211.87 $\pm$ 0.14	214.15	1.08	0.89	7.29		
35	423.15	0.6	$71.84\pm0.01$	$168.52 \pm 0.08$	169.72	1.11	0.91	7.70		
35	423.15	0.7	$72.31\pm0.01$	$128.36 \pm 0.06$	128.76	1.13	0.92	8.04		
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	$n^3$ ]		Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
35	423.15	0.8	$72.71\pm0.01$	$89.99 \pm 0.06$	90.21	1.15	0.93	8.31		
35	423.15	0.9	$72.86\pm0.01$	$53.37 \pm 0.03$	53.28	1.16	0.94	8.52		
35	423.15	1.0	$72.89\pm0.04$	$17.29 \pm 0.03$	17.27	1.16	0.95	8.67		
40	323.15	0.0	$54.34 \pm 0.01$	$910.98 \pm 0.22$	923.33	0.72	0.96	-3.37		
40	323.15	0.1	$55.17\pm0.01$	$787.52 \pm 0.23$	771.80	0.75	0.97	-1.47		
40	323.15	0.2	$56.40\pm0.01$	$659.29 \pm 0.45$	638.61	0.80	0.98	0.28		
40	323.15	0.3	$57.97\pm0.02$	$535.40 \pm 0.44$	520.84	0.87	0.99	1.78		
40	323.15	0.4	$59.63\pm0.02$	$426.27 \pm 0.41$	418.17	0.95	1.00	3.04		
40	323.15	0.5	$61.18\pm0.01$	$333.79 \pm 0.15$	330.08	1.03	1.00	4.03		
40	323.15	0.6	$62.43 \pm 0.03$	$256.74 \pm 0.40$	254.52	1.09	1.01	4.83		
40	323.15	0.7	$63.46 \pm 0.01$	$189.88 \pm 0.11$	188.70	1.15	1.01	5.44		
40	323.15	0.8	$64.23\pm0.01$	$130.55 \pm 0.05$	129.81	1.19	1.02	5.91		
40	323.15	0.9	$64.70\pm0.01$	$76.22 \pm 0.04$	75.61	1.21	1.02	6.25		
40	323.15	1.0	$64.93\pm0.01$	$24.45 \pm 0.01$	24.28	1.23	1.03	6.50		
40	348.15	0.0	$56.12 \pm 0.01$	$827.03 \pm 0.55$	839.93	0.74	1.03	-1.70		
40	348.15	0.1	$57.26 \pm 0.01$	$704.14 \pm 0.23$	697.55	0.78	1.03	0.09		
40	348.15	0.2	$58.76 \pm 0.01$	$582.93 \pm 0.35$	574.58	0.84	1.03	1.67		
40	348.15	0.3	$60.37\pm0.01$	$474.25 \pm 0.06$	468.67	0.92	0.91	2.98		
40	348.15	0.4	$61.93\pm0.02$	$380.42 \pm 0.33$	378.17	0.99	0.92	4.05		
40	348.15	0.5	$63.25 \pm 0.02$	$302.03 \pm 0.25$	300.85	1.05	0.93	4.90		
40	348.15	0.6	$64.33 \pm 0.02$	$234.66 \pm 0.20$	233.98	1.11	0.94	5.57		
40	348.15	0.7	$65.19\pm0.01$	$175.21 \pm 0.11$	174.78	1.15	0.95	6.10		
40	348.15	0.8	$65.80 \pm 0.01$	$121.40 \pm 0.05$	120.98	1.19	0.96	6.51		
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p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m <sup>3</sup> ]			Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
40	348.15	0.9	$66.18 \pm 0.01$	$71.22 \pm 0.01$	70.81	1.21	0.96	6.82		
40	348.15	1.0	$66.33\pm0.02$	$22.94 \pm 0.03$	22.82	1.21	0.97	7.04		
40	373.15	0.0	$58.19\pm0.01$	$741.73 \pm 0.39$	756.66	0.77	0.98	-0.08		
40	373.15	0.1	$59.57\pm0.01$	$625.53 \pm 0.36$	626.81	0.82	0.99	1.55		
40	373.15	0.2	$61.14\pm0.04$	$517.54 \pm 1.06$	516.96	0.89	0.99	2.93		
40	373.15	0.3	$62.65 \pm 0.01$	$424.31 \pm 0.25$	423.84	0.95	1.00	4.06		
40	373.15	0.4	$64.00\pm0.01$	$344.74 \pm 0.22$	344.61	1.02	1.01	4.96		
40	373.15	0.5	$65.20\pm0.01$	$275.80 \pm 0.09$	276.50	1.08	1.01	5.69		
40	373.15	0.6	$66.10\pm0.01$	$216.37 \pm 0.12$	216.69	1.12	1.02	6.27		
40	373.15	0.7	$66.77\pm0.01$	$163.01 \pm 0.06$	162.93	1.16	1.02	6.74		
40	373.15	0.8	$67.29 \pm 0.01$	$113.53 \pm 0.06$	113.36	1.18	1.02	7.10		
40	373.15	0.9	$67.58 \pm 0.01$	$66.88 \pm 0.02$	66.62	1.20	1.03	7.38		
40	373.15	1.0	$67.69\pm0.02$	$21.59 \pm 0.02$	21.53	1.20	1.03	7.58		
40	398.15	0.0	$60.44 \pm 0.03$	$662.11 \pm 0.91$	677.62	0.80	1.03	1.43		
40	398.15	0.1	$61.96\pm0.03$	$555.88 \pm 0.91$	563.19	0.87	1.03	2.87		
40	398.15	0.2	$63.45 \pm 0.02$	$463.03 \pm 0.44$	467.25	0.93	0.67	4.05		
40	398.15	0.3	$64.81\pm0.01$	$383.13 \pm 0.19$	386.12	0.99	0.71	5.01		
40	398.15	0.4	$65.96 \pm 0.01$	$314.87 \pm 0.21$	316.61	1.04	0.75	5.79		
40	398.15	0.5	$66.94\pm0.02$	$254.84 \pm 0.19$	256.02	1.09	0.79	6.42		
40	398.15	0.6	$67.69\pm0.02$	$201.42 \pm 0.15$	202.00	1.13	0.82	6.94		
40	398.15	0.7	$68.28\pm0.01$	$152.45 \pm 0.06$	152.70	1.16	0.85	7.35		
40	398.15	0.8	$68.67\pm0.01$	$106.81 \pm 0.06$	106.70	1.18	0.87	7.68		
40	398.15	0.9	$68.91\pm0.01$	$63.07 \pm 0.01$	62.91	1.19	0.90	7.94		
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$		
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]		
40	398.15	1.0	$68.96 \pm 0.01$	$20.41 \pm 0.01$	20.38	1.19	0.92	8.12		
40	423.15	0.0	$62.74 \pm 0.01$	$591.71 \pm 0.12$	607.12	0.85	0.93	2.80		
40	423.15	0.1	$64.21\pm0.04$	$499.50 \pm 1.01$	508.45	0.91	0.95	4.04		
40	423.15	0.2	$65.61\pm0.02$	$418.71 \pm 0.34$	425.44	0.97	0.97	5.06		
40	423.15	0.3	$66.78\pm0.03$	$350.23 \pm 0.47$	354.58	1.02	0.98	5.88		
40	423.15	0.4	$67.78\pm0.03$	$290.22 \pm 0.34$	293.10	1.07	0.99	6.56		
40	423.15	0.5	$68.61\pm0.02$	$236.67 \pm 0.18$	238.64	1.11	1.00	7.12		
40	423.15	0.6	$69.20\pm0.02$	$188.51 \pm 0.17$	189.35	1.13	1.01	7.58		
40	423.15	0.7	$69.68 \pm 0.01$	$143.46 \pm 0.07$	143.79	1.16	1.02	7.95		
40	423.15	0.8	$70.01\pm0.01$	$100.81 \pm 0.05$	100.83	1.17	1.03	8.25		
40	423.15	0.9	$70.17\pm0.02$	$59.74 \pm 0.05$	59.62	1.18	1.03	8.49		
40	423.15	1.0	$70.20\pm0.01$	$19.35 \pm 0.01$	19.36	1.18	1.04	8.66		
45	323.15	0.0	$53.97\pm0.01$	$929.81 \pm 0.35$	944.10	0.79	1.04	-3.58		
45	323.15	0.1	$54.58 \pm 0.01$	$813.27 \pm 0.25$	795.72	0.82	0.77	-1.72		
45	323.15	0.2	$55.55 \pm 0.01$	$690.02 \pm 0.46$	665.50	0.86	0.80	-0.00		
45	323.15	0.3	$56.80\pm0.02$	$569.36 \pm 0.51$	549.52	0.92	0.82	1.51		
45	323.15	0.4	$58.19\pm0.01$	$458.77 \pm 0.15$	446.44	0.99	0.85	2.78		
45	323.15	0.5	$59.48 \pm 0.03$	$363.21 \pm 0.49$	355.76	1.06	0.87	3.82		
45	323.15	0.6	$60.65\pm0.01$	$280.05 \pm 0.16$	276.17	1.13	0.89	4.66		
45	323.15	0.7	$61.58 \pm 0.02$	$207.88 \pm 0.20$	205.63	1.18	0.91	5.32		
45	323.15	0.8	$62.29\pm0.01$	$143.11 \pm 0.02$	141.88	1.22	0.92	5.83		
45	323.15	0.9	$62.73 \pm 0.01$	$83.61 \pm 0.05$	82.83	1.25	0.94	6.21		
45	323.15	1.0	$62.92\pm0.02$	$26.88 \pm 0.03$	26.66	1.26	0.95	6.48		
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
45	348.15	0.0	$55.56 \pm 0.02$	$852.22 \pm 0.87$	866.91	0.80	0.97	-1.98	
45	348.15	0.1	$56.44 \pm 0.01$	$735.24 \pm 0.42$	727.29	0.84	0.98	-0.21	
45	348.15	0.2	$57.60\pm0.01$	$618.98 \pm 0.36$	606.03	0.89	0.99	1.34	
45	348.15	0.3	$58.92\pm0.02$	$509.89 \pm 0.60$	499.92	0.96	1.00	2.69	
45	348.15	0.4	$60.25\pm0.02$	$413.28 \pm 0.50$	407.17	1.02	1.01	3.80	
45	348.15	0.5	$61.42 \pm 0.03$	$329.90 \pm 0.44$	326.21	1.08	1.01	4.69	
45	348.15	0.6	$62.42 \pm 0.01$	$256.88 \pm 0.08$	254.88	1.14	1.02	5.42	
45	348.15	0.7	$63.22\pm0.02$	$192.09 \pm 0.17$	190.99	1.18	1.03	6.00	
45	348.15	0.8	$63.78 \pm 0.01$	$133.30 \pm 0.08$	132.51	1.21	1.03	6.45	
45	348.15	0.9	$64.12\pm0.01$	$78.29 \pm 0.03$	77.70	1.23	1.03	6.78	
45	348.15	1.0	$64.26\pm0.01$	$25.23 \pm 0.02$	25.09	1.24	1.04	7.02	
45	373.15	0.0	$57.36 \pm 0.01$	$774.60 \pm 0.08$	790.38	0.82	0.83	-0.42	
45	373.15	0.1	$58.43 \pm 0.02$	$662.77 \pm 0.58$	661.72	0.87	0.85	1.19	
45	373.15	0.2	$59.70\pm0.01$	$555.92 \pm 0.16$	551.40	0.93	0.87	2.59	
45	373.15	0.3	$61.01\pm0.03$	$459.31 \pm 0.57$	456.17	0.99	0.88	3.76	
45	373.15	0.4	$62.18 \pm 0.01$	$375.85 \pm 0.26$	373.46	1.05	0.90	4.72	
45	373.15	0.5	$63.22\pm0.02$	$302.42 \pm 0.23$	301.08	1.10	0.92	5.50	
45	373.15	0.6	$64.07\pm0.03$	$237.55 \pm 0.36$	236.76	1.15	0.93	6.13	
45	373.15	0.7	$64.72\pm0.01$	$179.05 \pm 0.03$	178.42	1.18	0.94	6.63	
45	373.15	0.8	$65.20\pm0.02$	$124.82 \pm 0.10$	124.38	1.21	0.96	7.04	
45	373.15	0.9	$65.44 \pm 0.01$	$73.65 \pm 0.02$	73.20	1.22	0.97	7.35	
45	373.15	1.0	$65.52 \pm 0.03$	$23.80 \pm 0.03$	23.71	1.23	0.98	7.56	
45       398.15       0.0       59.30 $\pm$ 0.02       701.05 $\pm$ 0.74       717.19       0.85       0.99       1.04									
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p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
45	398.15	0.1	$60.49 \pm 0.03$	$597.33 \pm 0.74$	601.45	0.91	1.00	2.48	
45	398.15	0.2	$61.79\pm0.02$	$501.23 \pm 0.47$	503.08	0.97	1.00	3.72	
45	398.15	0.3	$62.97\pm0.01$	$417.82 \pm 0.29$	418.41	1.02	1.01	4.73	
45	398.15	0.4	$64.03 \pm 0.01$	$344.28 \pm 0.04$	344.72	1.07	1.02	5.57	
45	398.15	0.5	$64.88\pm0.01$	$279.80 \pm 0.15$	279.70	1.12	1.02	6.25	
45	398.15	0.6	$65.61 \pm 0.01$	$221.27 \pm 0.13$	221.20	1.16	1.03	6.81	
45	398.15	0.7	$66.14 \pm 0.01$	$167.76 \pm 0.10$	167.52	1.18	1.03	7.26	
45	398.15	0.8	$66.51 \pm 0.01$	$117.55 \pm 0.03$	117.23	1.20	1.03	7.62	
45	398.15	0.9	$66.72\pm0.03$	$69.50 \pm 0.09$	69.22	1.22	1.04	7.90	
45	398.15	1.0	$66.73 \pm 0.01$	$22.53 \pm 0.01$	22.47	1.22	0.87	8.10	
45	423.15	0.0	$61.35 \pm 0.01$	$633.03 \pm 0.32$	650.34	0.89	0.88	2.39	
45	423.15	0.1	$62.54 \pm 0.01$	$540.49 \pm 0.33$	548.22	0.94	0.90	3.65	
45	423.15	0.2	$63.69\pm0.01$	$457.86 \pm 0.07$	461.30	0.99	0.91	4.73	
45	423.15	0.3	$64.76 \pm 0.03$	$384.13 \pm 0.45$	386.15	1.05	0.92	5.61	
45	423.15	0.4	$65.70\pm0.01$	$318.66 \pm 0.12$	320.20	1.09	0.94	6.35	
45	423.15	0.5	$66.47\pm0.01$	$260.26 \pm 0.06$	261.34	1.13	0.95	6.96	
45	423.15	0.6	$67.04 \pm 0.01$	$207.35 \pm 0.10$	207.73	1.16	0.96	7.46	
45	423.15	0.7	$67.50 \pm 0.02$	$157.83 \pm 0.11$	157.98	1.18	0.97	7.87	
45	423.15	0.8	$67.78\pm0.01$	$111.09 \pm 0.02$	110.93	1.20	0.98	8.20	
45	423.15	0.9	$67.94\pm0.01$	$65.81 \pm 0.01$	65.67	1.21	0.99	8.45	
45	423.15	1.0	$67.93 \pm 0.01$	$21.36 \pm 0.01$	21.36	1.21	1.00	8.64	
50	323.15	0.0	$53.64\pm0.01$	947.08 $\pm$ 0.62	962.45	0.86	1.00	-3.79	
50	50       323.15       0.1       54.09 $\pm$ 0.01       835.23 $\pm$ 0.35       816.42       0.89       1.01       -1.95								
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p	Т	$x_{\mathrm{H}_2}$	L	$\rho$ / [kg/m	1 <sup>3</sup> ]		Ζ	$E_{\rm tot}$	
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]	
50	323.15	0.2	$54.84 \pm 0.01$	$717.14 \pm 0.39$	688.40	0.92	1.01	-0.25	
50	323.15	0.3	$55.83\pm0.01$	$599.43 \pm 0.11$	573.90	0.98	1.02	1.26	
50	323.15	0.4	$57.00\pm0.01$	$487.91 \pm 0.18$	470.82	1.04	1.02	2.55	
50	323.15	0.5	$58.14\pm0.01$	$388.93 \pm 0.10$	378.43	1.10	1.03	3.64	
50	323.15	0.6	$59.16 \pm 0.02$	$301.78 \pm 0.24$	295.70	1.16	1.03	4.52	
50	323.15	0.7	$59.99\pm0.01$	$224.79 \pm 0.12$	221.23	1.21	1.03	5.22	
50	323.15	0.8	$60.65 \pm 0.01$	$155.07 \pm 0.01$	153.15	1.25	1.03	5.76	
50	323.15	0.9	$61.05\pm0.01$	$90.70 \pm 0.02$	89.64	1.28	0.90	6.17	
50	323.15	1.0	$61.23\pm0.01$	$29.16 \pm 0.01$	28.93	1.29	0.91	6.45	
50	348.15	0.0	$55.07\pm0.01$	$875.04 \pm 0.58$	890.10	0.87	0.92	-2.24	
50	348.15	0.1	$55.73 \pm 0.01$	$763.72 \pm 0.54$	752.45	0.90	0.93	-0.49	
50	348.15	0.2	$56.68 \pm 0.01$	$649.63 \pm 0.45$	632.63	0.95	0.94	1.06	
50	348.15	0.3	$57.78\pm0.01$	$540.80 \pm 0.34$	526.68	1.00	0.95	2.43	
50	348.15	0.4	$58.91\pm0.02$	$442.07 \pm 0.47$	432.59	1.06	0.96	3.58	
50	348.15	0.5	$59.94\pm0.01$	$354.87 \pm 0.18$	348.90	1.12	0.97	4.52	
50	348.15	0.6	$60.83 \pm 0.01$	$277.53 \pm 0.04$	273.97	1.17	0.98	5.28	
50	348.15	0.7	$61.55 \pm 0.02$	$208.16 \pm 0.23$	206.04	1.21	0.99	5.90	
50	348.15	0.8	$62.07\pm0.01$	$144.63 \pm 0.10$	143.33	1.24	0.99	6.38	
50	348.15	0.9	$62.39\pm0.01$	$84.98 \pm 0.03$	84.24	1.26	1.00	6.75	
50	348.15	1.0	$62.51 \pm 0.01$	$27.41 \pm 0.01$	27.27	1.27	1.01	7.00	
50	373.15	0.0	$56.69\pm0.01$	$802.05 \pm 0.53$	818.76	0.88	1.01	-0.72	
50	373.15	0.1	$57.54 \pm 0.01$	$694.06 \pm 0.53$	691.10	0.92	1.02	0.88	
50	373.15	0.2	$58.57\pm0.02$	$588.56 \pm 0.67$	580.82	0.98	1.02	2.30	
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p	Т	$x_{\mathrm{H}_2}$	L	ho / [kg/m <sup>3</sup> ]		Z		$E_{\rm tot}$
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]
50	373.15	0.3	$59.64\pm0.02$	$491.70 \pm 0.61$	484.28	1.03	1.02	3.50
50	373.15	0.4	$60.70\pm0.02$	$404.14 \pm 0.35$	399.12	1.09	1.03	4.50
50	373.15	0.5	$61.61\pm0.02$	$326.78 \pm 0.36$	323.42	1.13	1.03	5.33
50	373.15	0.6	$62.38 \pm 0.01$	$257.45 \pm 0.11$	255.27	1.18	1.03	6.00
50	373.15	0.7	$63.00 \pm 0.01$	$194.10 \pm 0.03$	192.92	1.21	1.03	6.55
50	373.15	0.8	$63.44\pm0.01$	$135.50 \pm 0.01$	134.76	1.24	0.63	6.98
50	373.15	0.9	$63.65 \pm 0.01$	$80.03 \pm 0.04$	79.47	1.25	0.69	7.31
50	373.15	1.0	$63.71 \pm 0.01$	$25.89 \pm 0.01$	25.79	1.25	0.73	7.54
50	398.15	0.0	$58.40\pm0.02$	$733.85 \pm 0.68$	750.33	0.91	0.77	0.69
50	398.15	0.1	$59.39\pm0.01$	$631.29 \pm 0.35$	634.01	0.95	0.81	2.16
50	398.15	0.2	$60.40\pm0.01$	$536.72 \pm 0.27$	534.06	1.00	0.84	3.41
50	398.15	0.3	$61.45 \pm 0.01$	$449.60 \pm 0.05$	446.96	1.06	0.86	4.47
50	398.15	0.4	$62.39\pm0.02$	$372.09 \pm 0.29$	370.08	1.10	0.89	5.36
50	398.15	0.5	$63.20\pm0.01$	$302.78 \pm 0.19$	301.40	1.15	0.91	6.09
50	398.15	0.6	$63.85\pm0.01$	$240.07 \pm 0.02$	239.06	1.18	0.93	6.69
50	398.15	0.7	$64.36 \pm 0.01$	$182.03 \pm 0.08$	181.45	1.21	0.95	7.18
50	398.15	0.8	$64.69\pm0.01$	$127.76 \pm 0.05$	127.22	1.23	0.96	7.57
50	398.15	0.9	$64.86 \pm 0.01$	$75.66 \pm 0.02$	75.24	1.24	0.98	7.87
50	398.15	1.0	$64.88 \pm 0.02$	$24.52 \pm 0.02$	24.47	1.24	0.99	8.09
50	423.15	0.0	$60.21\pm0.01$	$669.62 \pm 0.26$	686.95	0.93	1.00	2.02
50	423.15	0.1	$61.21\pm0.01$	$576.58 \pm 0.34$	582.58	0.98	1.01	3.32
50	423.15	0.2	$62.18\pm0.03$	$491.99 \pm 0.60$	492.86	1.03	1.02	4.43
50	423.15	0.3	$63.15\pm0.03$	$414.32 \pm 0.54$	414.48	1.08	1.03	5.37
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p	T	$x_{\mathrm{H}_2}$	L	ho / [kg/m <sup>3</sup> ]		Z		$E_{\rm tot}$
[MPa]	[K]		[Å]	$ ho^{ m MD}$	$ ho^{ m RFP}$	$Z^{\mathrm{MD}}$	$Z^{\rm RFP}$	[kJ/mol]
50	423.15	0.4	$63.96 \pm 0.01$	$345.34 \pm 0.23$	344.94	1.12	1.03	6.15
50	423.15	0.5	$64.66 \pm 0.01$	$282.68 \pm 0.07$	282.32	1.16	1.04	6.80
50	423.15	0.6	$65.23 \pm 0.02$	$225.15 \pm 0.20$	224.93	1.19	1.04	7.35
50	423.15	0.7	$65.63\pm0.02$	$171.70 \pm 0.16$	171.36	1.21	0.75	7.79
50	423.15	0.8	$65.89\pm0.01$	$120.89 \pm 0.04$	120.52	1.22	0.78	8.15
50	423.15	0.9	$66.02\pm0.02$	$71.75 \pm 0.05$	71.46	1.23	0.81	8.43
50	423.15	1.0	$65.98 \pm 0.02$	$23.31 \pm 0.02$	23.29	1.23	0.83	8.63

#### <sup>189</sup> S10.2 Thermodynamic factors, viscosities, self-diffusion, Maxwell-

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#### Stefan and Fick diffusion coefficients

Table S3: Viscosities  $(\eta)$ , thermodynamic factors  $(\Gamma)$ , self-diffusion coefficients  $(D^{\text{self}})$  of CO<sub>2</sub> and H<sub>2</sub>, Maxwell-Stefan diffusion coefficients  $(D^{\text{MS}})$ , and Fick diffusion coefficients obtained from MD simulations of CO<sub>2</sub>-H<sub>2</sub> mixtures comprising of 120 molecules are presented as functions of pressure, temperature, and mole fraction of H<sub>2</sub>. The viscosity predictions from REFPROP<sup>3</sup>  $(\eta^{\text{RFP}})$  are provided for comparison. The tabulated self-, Maxwell-Stefan (MS), and Fick diffusion coefficients have been corrected for finite-size effects using Eqs. 1, 2, and 4 of the main text, respectively. The average box lengths of the cubic simulation boxes with 120 molecules follow from the densities provided in Table S2.

p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu  ext{Pa}]$	as]	$D^{\text{self}} / [10^{-8} \text{m}^2/\text{s}]$		$D^{\text{self}} / [10^{-8} \text{m}^2/\text{s}]$		$[0^{-8} m^2/s]$ $D^{MS}$	
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} \text{m}^2/\text{s}]$	$[10^{-6} {\rm m}^2/{\rm s}]$		
5	323.15	0.0	1.00	$16.0 \pm 2.8$	17.3	21.92	-	-	-		
5	323.15	0.1	0.96	$16.9\pm0.6$	17.1	25.26	134.96	$1.24 \pm 0.04$	$1.20\pm0.04$		
5	323.15	0.2	0.93	$17.3 \pm 1.9$	16.8	28.67	145.08	$1.26 \pm 0.01$	$1.18\pm0.01$		
5	323.15	0.3	0.91	$16.8 \pm 1.9$	16.6	32.74	160.19	$1.34 \pm 0.03$	$1.23\pm0.03$		
5	323.15	0.4	0.91	$15.8\pm0.2$	16.4	37.04	177.09	$1.36 \pm 0.06$	$1.23\pm0.05$		
5	323.15	0.5	0.90	$16.3\pm0.8$	16.1	43.92	194.10	$1.37 \pm 0.35$	$1.24 \pm 0.32$		
5	323.15	0.6	0.91	$15.7\pm0.4$	15.8	51.30	214.42	$1.44 \pm 0.05$	$1.31\pm0.05$		
5	323.15	0.7	0.92	$14.4 \pm 1.0$	15.4	61.78	237.97	$1.52\pm0.09$	$1.40\pm0.09$		
5	323.15	0.8	0.94	$14.0 \pm 1.1$	14.6	75.43	264.68	$1.41 \pm 0.02$	$1.33\pm0.02$		
5	323.15	0.9	0.97	$12.2 \pm 0.3$	13.2	95.20	296.24	$1.35 \pm 0.03$	$1.30\pm0.02$		
5	323.15	1.0	1.00	$9.7 \pm 1.1$	9.5	-	332.34	-	-		
5	348.15	0.0	1.00	$17.5\pm0.4$	18.3	26.90	-	-	-		
5	348.15	0.1	0.98	$17.5\pm0.5$	18.1	30.25	155.38	$1.50 \pm 0.08$	$1.47\pm0.07$		
5	348.15	0.2	0.96	$18.0 \pm 1.3$	17.8	34.27	170.83	$1.51 \pm 0.08$	$1.45 \pm 0.08$		
Continued on next page											
p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} \text{m}^2/\text{s}]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$		
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[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} \text{m}^2/\text{s}]$	$[10^{-6} {\rm m}^2/{\rm s}]$		
5	348.15	0.3	0.94	$16.7\pm0.6$	17.6	39.20	185.94	$1.46 \pm 0.02$	$1.38 \pm 0.02$		
5	348.15	0.4	0.93	$15.8 \pm 1.1$	17.4	44.70	203.92	$1.56 \pm 0.07$	$1.45 \pm 0.06$		
5	348.15	0.5	0.93	$17.9 \pm 2.0$	17.1	51.11	224.04	$1.60 \pm 0.06$	$1.49 \pm 0.06$		
5	348.15	0.6	0.93	$17.6 \pm 1.1$	16.8	60.11	247.74	$1.64\pm0.01$	$1.52 \pm 0.01$		
5	348.15	0.7	0.94	$14.7\pm0.8$	16.3	72.09	275.79	$1.67 \pm 0.11$	$1.56 \pm 0.10$		
5	348.15	0.8	0.95	$14.6\pm0.5$	15.5	88.64	300.38	$1.76 \pm 0.16$	$1.67 \pm 0.15$		
5	348.15	0.9	0.97	$12.7\pm0.8$	13.9	108.69	335.95	$1.67\pm0.03$	$1.62\pm0.03$		
5	348.15	1.0	1.00	$9.7\pm0.5$	10.0	-	370.68	-	-		
5	373.15	0.0	1.00	$18.2\pm0.7$	19.3	31.52	-	-	-		
5	373.15	0.1	0.98	$21.2 \pm 4.9$	19.1	35.45	178.60	$1.67\pm0.01$	$1.64\pm0.01$		
5	373.15	0.2	0.97	$18.4\pm0.6$	18.9	40.07	193.15	$1.74 \pm 0.02$	$1.69\pm0.02$		
5	373.15	0.3	0.96	$17.8\pm0.8$	18.7	45.41	216.39	$1.87 \pm 0.09$	$1.79\pm0.09$		
5	373.15	0.4	0.95	$17.6\pm0.4$	18.4	50.72	232.03	$1.86 \pm 0.07$	$1.76 \pm 0.07$		
5	373.15	0.5	0.94	$17.8\pm0.2$	18.1	58.00	253.51	$1.82 \pm 0.01$	$1.72 \pm 0.01$		
5	373.15	0.6	0.94	$17.4 \pm 0.7$	17.8	67.84	280.37	$1.84 \pm 0.08$	$1.74 \pm 0.08$		
5	373.15	0.7	0.95	$16.4 \pm 1.1$	17.2	79.83	307.12	$2.06 \pm 0.34$	$1.95\pm0.32$		
5	373.15	0.8	0.96	$15.6 \pm 1.3$	16.3	98.54	343.77	$1.96 \pm 0.27$	$1.88 \pm 0.25$		
5	373.15	0.9	0.98	$13.2 \pm 1.3$	14.6	127.45	382.58	$1.69 \pm 0.09$	$1.65 \pm 0.09$		
5	373.15	1.0	1.00	$10.2\pm0.7$	10.5	-	423.91	-	-		
5	398.15	0.0	1.00	$20.0\pm0.7$	20.3	37.18	-	-	-		
5	398.15	0.1	0.99	$20.4 \pm 1.2$	20.1	42.28	202.56	$1.89 \pm 0.06$	$1.87 \pm 0.06$		
5	398.15	0.2	0.98	$20.9 \pm 1.2$	19.9	45.42	228.84	$1.96 \pm 0.05$	$1.92 \pm 0.05$		
5	398.15	0.3	0.97	$19.2 \pm 1.0$	19.7	52.07	242.25	$2.09 \pm 0.10$	$2.03 \pm 0.09$		
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} \text{m}^2/\text{s}]$	$[10^{-6} {\rm m}^2/{\rm s}]$
5	398.15	0.4	0.96	$16.9 \pm 3.2$	19.5	58.77	263.13	$1.93 \pm 0.06$	$1.86\pm0.06$
5	398.15	0.5	0.95	$17.9\pm0.8$	19.1	67.64	283.38	$2.01 \pm 0.06$	$1.92\pm0.06$
5	398.15	0.6	0.95	$17.1 \pm 1.5$	18.7	78.31	312.91	$2.12 \pm 0.07$	$2.02 \pm 0.06$
5	398.15	0.7	0.96	$18.3 \pm 1.5$	18.1	90.45	345.28	$2.10\pm0.07$	$2.01 \pm 0.07$
5	398.15	0.8	0.96	$16.8 \pm 1.2$	17.1	108.75	372.84	$2.04 \pm 0.05$	$1.96 \pm 0.04$
5	398.15	0.9	0.98	$14.8 \pm 1.1$	15.3	139.93	426.12	$2.22 \pm 0.06$	$2.17\pm0.06$
5	398.15	1.0	1.00	$10.7 \pm 1.0$	10.9	-	471.04	-	-
5	423.15	0.0	1.00	$20.1 \pm 1.1$	21.3	42.27	-	-	-
5	423.15	0.1	0.99	$20.6\pm0.9$	21.1	46.67	224.49	$2.16 \pm 0.03$	$2.15 \pm 0.03$
5	423.15	0.2	0.98	$17.5 \pm 6.2$	21.0	52.27	249.24	$2.17\pm0.01$	$2.14 \pm 0.01$
5	423.15	0.3	0.98	$19.6\pm0.4$	20.7	59.24	272.64	$2.33 \pm 0.05$	$2.27\pm0.05$
5	423.15	0.4	0.97	$21.3 \pm 2.0$	20.5	67.23	289.44	$2.32 \pm 0.12$	$2.25 \pm 0.11$
5	423.15	0.5	0.96	$20.0 \pm 1.4$	20.1	75.59	314.57	$2.27 \pm 0.13$	$2.19 \pm 0.13$
5	423.15	0.6	0.96	$18.5\pm0.9$	19.7	85.74	352.51	$2.28 \pm 0.03$	$2.19\pm0.03$
5	423.15	0.7	0.96	$17.9 \pm 1.5$	19.0	101.81	376.94	$2.36 \pm 0.21$	$2.27\pm0.21$
5	423.15	0.8	0.97	$17.0 \pm 1.2$	17.9	123.77	420.83	$2.22 \pm 0.04$	$2.15\pm0.04$
5	423.15	0.9	0.98	$14.7 \pm 2.1$	16.0	153.43	480.22	$2.36 \pm 0.11$	$2.31\pm0.11$
5	423.15	1.0	1.00	$10.8\pm0.8$	11.4	-	520.37	-	-
10	323.15	0.0	1.00	$25.5\pm0.9$	28.4	6.20	-	-	-
10	323.15	0.1	0.85	$19.7\pm0.2$	21.2	10.22	46.91	$0.45 \pm 0.01$	$0.39\pm0.01$
10	323.15	0.2	0.77	$18.1\pm0.6$	19.3	12.87	59.74	$0.55\pm0.01$	$0.42 \pm 0.01$
10	323.15	0.3	0.72	$17.3\pm0.2$	18.3	15.44	70.49	$0.64 \pm 0.06$	$0.47 \pm 0.04$
10	323.15	0.4	0.72	$17.0\pm0.6$	17.6	18.39	82.12	$0.64\pm0.01$	$0.47\pm0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
10	323.15	0.5	0.75	$16.2 \pm 0.4$	17.1	21.64	91.59	$0.70 \pm 0.02$	$0.52 \pm 0.01$
10	323.15	0.6	0.80	$15.7\pm0.7$	16.5	25.94	103.77	$0.74\pm0.03$	$0.59\pm0.02$
10	323.15	0.7	0.85	$16.8 \pm 2.1$	15.9	31.25	116.98	$0.79\pm0.05$	$0.67\pm0.05$
10	323.15	0.8	0.91	$13.3\pm0.8$	15.0	38.66	131.79	$0.72\pm0.01$	$0.66\pm0.01$
10	323.15	0.9	0.97	$12.3\pm0.5$	13.4	50.20	149.38	$0.75\pm0.02$	$0.72 \pm 0.02$
10	323.15	1.0	1.00	$10.2 \pm 1.8$	9.6	-	166.46	-	-
10	348.15	0.0	1.00	$21.0\pm0.4$	22.2	10.90	-	-	-
10	348.15	0.1	0.93	$19.5\pm0.5$	20.6	13.48	63.53	$0.60\pm0.01$	$0.56\pm0.01$
10	348.15	0.2	0.88	$18.8\pm0.4$	19.7	15.93	73.46	$0.69\pm0.01$	$0.61 \pm 0.01$
10	348.15	0.3	0.85	$19.6 \pm 1.8$	19.0	18.75	85.18	$0.73 \pm 0.02$	$0.62\pm0.02$
10	348.15	0.4	0.83	$18.0\pm0.7$	18.5	21.85	95.53	$0.75\pm0.02$	$0.63\pm0.01$
10	348.15	0.5	0.83	$17.6 \pm 1.4$	18.0	25.42	107.30	$0.77\pm0.05$	$0.64\pm0.04$
10	348.15	0.6	0.85	$16.4\pm0.3$	17.4	29.96	118.14	$0.83 \pm 0.02$	$0.70\pm0.02$
10	348.15	0.7	0.88	$15.8\pm0.6$	16.7	35.99	133.49	$0.84\pm0.02$	$0.74\pm0.02$
10	348.15	0.8	0.91	$14.4\pm0.3$	15.8	43.64	150.66	$0.89\pm0.06$	$0.81\pm0.05$
10	348.15	0.9	0.95	$13.4 \pm 1.0$	14.1	55.04	170.38	$0.87\pm0.03$	$0.83\pm0.03$
10	348.15	1.0	1.00	$9.8 \pm 0.3$	10.1	-	189.67	-	-
10	373.15	0.0	1.00	$21.6\pm0.7$	21.8	14.07	-	-	-
10	373.15	0.1	0.96	$20.9 \pm 2.2$	21.0	16.65	77.96	$0.73\pm0.01$	$0.70\pm0.01$
10	373.15	0.2	0.92	$21.2 \pm 2.6$	20.3	19.27	88.73	$0.81\pm0.02$	$0.74\pm0.02$
10	373.15	0.3	0.90	$19.7 \pm 1.5$	19.8	22.35	98.83	$0.84\pm0.01$	$0.75 \pm 0.01$
10	373.15	0.4	0.88	$18.9 \pm 1.1$	19.3	25.76	111.48	$0.86 \pm 0.04$	$0.76\pm0.04$
10	373.15	0.5	0.88	$18.1\pm0.9$	18.9	29.55	122.08	$0.93\pm0.08$	$0.82\pm0.07$
				Contin	nued on	next pag	ge		

p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
10	373.15	0.6	0.88	$18.1 \pm 0.8$	18.3	34.05	136.30	$0.90\pm0.02$	$0.79\pm0.02$
10	373.15	0.7	0.90	$18.6 \pm 2.7$	17.6	41.78	151.76	$0.93\pm0.05$	$0.83\pm0.04$
10	373.15	0.8	0.92	$15.6\pm0.9$	16.6	50.72	169.05	$1.02 \pm 0.06$	$0.94\pm0.06$
10	373.15	0.9	0.96	$14.8 \pm 2.1$	14.8	63.15	192.91	$0.95\pm0.04$	$0.91\pm0.04$
10	373.15	1.0	1.00	$9.9 \pm 0.3$	10.6	-	212.76	-	-
10	398.15	0.0	1.00	$21.0 \pm 1.8$	22.2	17.24	-	-	-
10	398.15	0.1	0.97	$21.2 \pm 1.9$	21.6	19.68	91.91	$0.88\pm0.01$	$0.85\pm0.01$
10	398.15	0.2	0.95	$22.0 \pm 1.8$	21.1	22.25	101.59	$0.89\pm0.01$	$0.84\pm0.01$
10	398.15	0.3	0.93	$20.3 \pm 1.0$	20.7	25.34	113.95	$1.02 \pm 0.06$	$0.95\pm0.05$
10	398.15	0.4	0.91	$19.7\pm0.7$	20.2	28.83	125.96	$1.01 \pm 0.02$	$0.92\pm0.02$
10	398.15	0.5	0.90	$19.6 \pm 1.4$	19.8	33.32	137.76	$1.03 \pm 0.05$	$0.93\pm0.04$
10	398.15	0.6	0.90	$18.5\pm0.9$	19.2	39.29	154.84	$1.04 \pm 0.03$	$0.94\pm0.02$
10	398.15	0.7	0.91	$17.2\pm0.3$	18.5	45.86	169.54	$1.12 \pm 0.01$	$1.02 \pm 0.01$
10	398.15	0.8	0.93	$15.9\pm0.3$	17.4	57.28	189.93	$1.09 \pm 0.02$	$1.02 \pm 0.02$
10	398.15	0.9	0.96	$14.0\pm0.6$	15.4	69.30	212.05	$1.09 \pm 0.04$	$1.04\pm0.04$
10	398.15	1.0	1.00	$10.3\pm0.2$	11.0	-	236.14	-	-
10	423.15	0.0	1.00	$23.3 \pm 1.2$	22.8	19.99	-	-	-
10	423.15	0.1	0.98	$22.4 \pm 0.6$	22.4	22.90	104.34	$1.00 \pm 0.03$	$0.98\pm0.03$
10	423.15	0.2	0.96	$21.0\pm0.2$	22.0	25.57	116.03	$1.06 \pm 0.03$	$1.02 \pm 0.03$
10	423.15	0.3	0.94	$20.8\pm0.7$	21.6	28.91	129.73	$1.11 \pm 0.04$	$1.05 \pm 0.04$
10	423.15	0.4	0.93	$20.3\pm0.4$	21.2	33.17	141.51	$1.12 \pm 0.06$	$1.04 \pm 0.06$
10	423.15	0.5	0.92	$20.5\pm0.9$	20.7	37.63	157.07	$1.16 \pm 0.03$	$1.07 \pm 0.03$
10	423.15	0.6	0.92	$19.9 \pm 1.3$	20.1	43.09	173.19	$1.12 \pm 0.09$	$1.03 \pm 0.08$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu \mathrm{Pa}]$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H_2}}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
10	423.15	0.7	0.92	$18.4 \pm 1.1$	19.3	53.16	191.77	$1.17\pm0.01$	$1.08\pm0.01$
10	423.15	0.8	0.94	$17.2 \pm 1.1$	18.2	63.55	208.51	$1.16\pm0.01$	$1.09\pm0.01$
10	423.15	0.9	0.96	$16.1 \pm 1.6$	16.1	78.48	236.12	$1.18\pm0.02$	$1.13\pm0.02$
10	423.15	1.0	1.00	$11.2\pm0.5$	11.5	-	259.70	-	-
15	323.15	0.0	1.00	$57.7\pm0.7$	56.5	2.68	-	-	-
15	323.15	0.1	0.71	$32.0 \pm 3.1$	33.4	5.07	18.91	$0.18\pm0.01$	$0.13\pm0.01$
15	323.15	0.2	0.55	$23.1 \pm 1.0$	24.7	7.60	31.20	$0.29\pm0.01$	$0.16\pm0.01$
15	323.15	0.3	0.48	$19.3\pm0.8$	21.3	9.81	41.07	$0.37\pm0.01$	$0.18\pm0.01$
15	323.15	0.4	0.50	$18.1\pm0.5$	19.5	12.03	49.70	$0.42\pm0.01$	$0.21\pm0.01$
15	323.15	0.5	0.57	$17.4 \pm 0.7$	18.3	14.67	58.63	$0.45\pm0.01$	$0.26\pm0.01$
15	323.15	0.6	0.67	$17.4 \pm 2.3$	17.3	17.51	67.05	$0.48\pm0.01$	$0.32\pm0.01$
15	323.15	0.7	0.79	$15.6\pm0.8$	16.4	21.46	77.06	$0.51\pm0.01$	$0.40\pm0.01$
15	323.15	0.8	0.90	$14.2\pm0.4$	15.3	26.41	88.59	$0.52\pm0.01$	$0.47\pm0.01$
15	323.15	0.9	0.97	$12.3\pm0.3$	13.6	34.40	99.04	$0.53\pm0.02$	$0.52\pm0.02$
15	323.15	1.0	1.00	$9.4 \pm 0.4$	9.8	-	113.71	-	-
15	348.15	0.0	1.00	$32.0\pm0.5$	34.8	5.26	-	-	-
15	348.15	0.1	0.85	$25.3 \pm 2.9$	26.4	7.79	32.60	$0.31\pm0.01$	$0.26 \pm 0.01$
15	348.15	0.2	0.76	$20.4 \pm 1.0$	23.0	9.97	42.09	$0.39\pm0.01$	$0.29\pm0.01$
15	348.15	0.3	0.71	$20.0 \pm 1.1$	21.1	12.09	51.43	$0.44\pm0.01$	$0.32\pm0.01$
15	348.15	0.4	0.70	$19.6 \pm 1.1$	19.9	14.69	60.78	$0.50\pm0.02$	$0.35\pm0.01$
15	348.15	0.5	0.72	$18.5 \pm 1.0$	19.0	17.22	69.48	$0.54\pm0.03$	$0.39\pm0.02$
15	348.15	0.6	0.76	$17.3\pm0.5$	18.1	20.15	78.53	$0.55\pm0.03$	$0.42\pm0.02$
15	348.15	0.7	0.82	$16.9 \pm 0.5$	17.2	24.76	88.65	$0.58\pm0.01$	$0.47 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
15	348.15	0.8	0.88	$15.0 \pm 0.8$	16.1	30.22	100.80	$0.59\pm0.01$	$0.52 \pm 0.01$
15	348.15	0.9	0.95	$13.4\pm0.9$	14.3	40.47	113.52	$0.59\pm0.01$	$0.56\pm0.01$
15	348.15	1.0	1.00	$10.4\pm0.9$	10.2	-	127.84	-	-
15	373.15	0.0	1.00	$26.4 \pm 1.6$	27.8	8.14	-	-	-
15	373.15	0.1	0.92	$23.1\pm0.6$	24.6	10.19	43.44	$0.43 \pm 0.02$	$0.39\pm0.01$
15	373.15	0.2	0.86	$24.4 \pm 5.9$	22.7	12.31	52.53	$0.48\pm0.01$	$0.41\pm0.01$
15	373.15	0.3	0.82	$21.3 \pm 1.1$	21.5	14.41	61.57	$0.53\pm0.01$	$0.43\pm0.01$
15	373.15	0.4	0.80	$19.3\pm0.5$	20.5	17.01	69.69	$0.57\pm0.01$	$0.46\pm0.01$
15	373.15	0.5	0.80	$19.1\pm0.4$	19.7	19.73	79.58	$0.63 \pm 0.04$	$0.50\pm0.03$
15	373.15	0.6	0.82	$18.5\pm0.4$	18.9	23.35	89.33	$0.62\pm0.01$	$0.51\pm0.01$
15	373.15	0.7	0.85	$17.3\pm0.7$	18.0	28.13	100.31	$0.64\pm0.01$	$0.54\pm0.01$
15	373.15	0.8	0.89	$15.8\pm0.5$	16.9	34.55	113.37	$0.70\pm0.02$	$0.63\pm0.02$
15	373.15	0.9	0.94	$13.6\pm0.4$	14.9	43.93	128.79	$0.70\pm0.04$	$0.66\pm0.03$
15	373.15	1.0	1.00	$11.1 \pm 1.0$	10.7	-	143.91	-	-
15	398.15	0.0	1.00	$24.9\pm0.4$	26.0	10.46	-	-	-
15	398.15	0.1	0.95	$23.2 \pm 1.0$	24.2	12.47	54.41	$0.52\pm0.01$	$0.50\pm0.01$
15	398.15	0.2	0.91	$23.6 \pm 1.6$	23.0	14.56	62.72	$0.59\pm0.03$	$0.54\pm0.02$
15	398.15	0.3	0.87	$22.1\pm0.7$	22.1	16.96	71.49	$0.62\pm0.01$	$0.54\pm0.01$
15	398.15	0.4	0.86	$21.6 \pm 1.2$	21.3	19.59	80.36	$0.66 \pm 0.01$	$0.56\pm0.01$
15	398.15	0.5	0.85	$19.6\pm0.7$	20.5	22.75	90.30	$0.67\pm0.01$	$0.57\pm0.01$
15	398.15	0.6	0.85	$18.9 \pm 1.0$	19.8	27.22	100.31	$0.70\pm0.02$	$0.60 \pm 0.02$
15	398.15	0.7	0.87	$17.9\pm0.6$	18.9	31.69	112.90	$0.71\pm0.01$	$0.62\pm0.01$
15	398.15	0.8	0.90	$16.5\pm0.8$	17.6	39.02	126.34	$0.74\pm0.01$	$0.67\pm0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H_2}}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} m^2/s]$
15	398.15	0.9	0.94	$14.4 \pm 0.3$	15.6	49.63	144.12	$0.73 \pm 0.04$	$0.69\pm0.03$
15	398.15	1.0	1.00	$11.5 \pm 1.0$	11.1	-	158.95	-	-
15	423.15	0.0	1.00	$24.5\pm0.9$	25.6	12.65	-	-	-
15	423.15	0.1	0.96	$23.7\pm0.7$	24.4	14.68	64.13	$0.61\pm0.02$	$0.59\pm0.02$
15	423.15	0.2	0.93	$22.7\pm0.9$	23.5	16.80	72.71	$0.67\pm0.02$	$0.62\pm0.02$
15	423.15	0.3	0.91	$21.5\pm0.4$	22.7	19.19	82.02	$0.68\pm0.01$	$0.62\pm0.01$
15	423.15	0.4	0.89	$22.0\pm0.7$	22.1	21.99	91.29	$0.71\pm0.01$	$0.63\pm0.01$
15	423.15	0.5	0.88	$20.7\pm0.6$	21.4	25.26	102.28	$0.74\pm0.02$	$0.65\pm0.02$
15	423.15	0.6	0.88	$19.7\pm0.6$	20.6	29.44	113.81	$0.78\pm0.02$	$0.68\pm0.02$
15	423.15	0.7	0.89	$19.4\pm0.9$	19.7	35.44	126.36	$0.92\pm0.11$	$0.82\pm0.10$
15	423.15	0.8	0.91	$16.9\pm0.6$	18.4	44.01	141.19	$0.79\pm0.04$	$0.72\pm0.04$
15	423.15	0.9	0.95	$14.7\pm0.7$	16.2	54.42	159.56	$0.85\pm0.01$	$0.81\pm0.01$
15	423.15	1.0	1.00	$11.3\pm0.6$	11.6	-	182.40	-	-
20	323.15	0.0	1.00	$68.8\pm0.8$	68.7	2.24	-	-	-
20	323.15	0.1	0.68	$42.7 \pm 1.3$	44.9	3.49	11.32	$0.11\pm0.01$	$0.08\pm0.01$
20	323.15	0.2	0.49	$29.7 \pm 2.5$	31.7	5.24	19.05	$0.19\pm0.01$	$0.09\pm0.01$
20	323.15	0.3	0.40	$23.0\pm0.8$	25.2	7.07	27.48	$0.28\pm0.03$	$0.11 \pm 0.01$
20	323.15	0.4	0.40	$20.3\pm0.6$	21.8	8.90	34.91	$0.31\pm0.01$	$0.12\pm0.01$
20	323.15	0.5	0.47	$18.2\pm0.3$	19.8	11.06	41.95	$0.34\pm0.01$	$0.16\pm0.01$
20	323.15	0.6	0.57	$17.1\pm0.5$	18.3	13.20	49.60	$0.36\pm0.01$	$0.21 \pm 0.01$
20	323.15	0.7	0.70	$16.0\pm0.6$	17.0	16.19	57.26	$0.38\pm0.02$	$0.27\pm0.01$
20	323.15	0.8	0.83	$14.6\pm0.5$	15.7	20.84	65.94	$0.40\pm0.01$	$0.33 \pm 0.01$
20	323.15	0.9	0.94	$13.1 \pm 0.5$	13.8	28.53	76.47	$0.41\pm0.01$	$0.39\pm0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
20	323.15	1.0	1.00	$9.5 \pm 0.2$	9.9	-	86.03	-	-
20	348.15	0.0	1.00	$46.6\pm0.4$	49.1	3.52	-	-	-
20	348.15	0.1	0.80	$32.1 \pm 1.1$	34.7	5.26	19.18	$0.19\pm0.01$	$0.15\pm0.01$
20	348.15	0.2	0.67	$25.4 \pm 0.4$	27.7	7.13	27.65	$0.26\pm0.01$	$0.18\pm0.01$
20	348.15	0.3	0.61	$22.4 \pm 0.2$	24.0	9.02	35.06	$0.32\pm0.01$	$0.19\pm0.01$
20	348.15	0.4	0.60	$19.8\pm0.9$	21.7	10.82	42.94	$0.35\pm0.01$	$0.21\pm0.01$
20	348.15	0.5	0.63	$19.2 \pm 1.1$	20.2	13.11	50.32	$0.39\pm0.01$	$0.25\pm0.01$
20	348.15	0.6	0.68	$19.1 \pm 2.0$	18.9	15.63	57.04	$0.43\pm0.02$	$0.30\pm0.01$
20	348.15	0.7	0.76	$17.7 \pm 1.3$	17.8	18.84	65.99	$0.44\pm0.01$	$0.33\pm0.01$
20	348.15	0.8	0.85	$15.2 \pm 0.4$	16.4	24.11	75.04	$0.45\pm0.01$	$0.38\pm0.01$
20	348.15	0.9	0.93	$13.5\pm0.3$	14.5	30.44	86.87	$0.53\pm0.08$	$0.49\pm0.07$
20	348.15	1.0	1.00	$9.6\pm0.7$	10.3	-	97.03	-	-
20	373.15	0.0	1.00	$35.1\pm0.3$	37.2	5.34	-	-	-
20	373.15	0.1	0.88	$27.5\pm0.3$	30.0	7.17	27.38	$0.27\pm0.01$	$0.23\pm0.01$
20	373.15	0.2	0.79	$24.6\pm0.7$	26.1	8.96	35.23	$0.34\pm0.01$	$0.27\pm0.01$
20	373.15	0.3	0.74	$22.4 \pm 0.5$	23.7	10.82	43.27	$0.38\pm0.01$	$0.28\pm0.01$
20	373.15	0.4	0.72	$20.9\pm0.6$	22.0	12.84	50.12	$0.41 \pm 0.01$	$0.30\pm0.01$
20	373.15	0.5	0.73	$19.7\pm0.6$	20.8	15.24	57.56	$0.45\pm0.02$	$0.33\pm0.01$
20	373.15	0.6	0.76	$19.0\pm0.4$	19.6	18.10	66.62	$0.52\pm0.06$	$0.40\pm0.05$
20	373.15	0.7	0.80	$18.0 \pm 1.1$	18.5	21.74	75.40	$0.51\pm0.02$	$0.41 \pm 0.01$
20	373.15	0.8	0.86	$16.0\pm0.7$	17.1	27.71	85.63	$0.50\pm0.01$	$0.43 \pm 0.01$
20	373.15	0.9	0.93	$13.9 \pm 1.2$	15.1	34.69	97.16	$0.51\pm0.02$	$0.48 \pm 0.02$
20	373.15	1.0	1.00	$10.7\pm0.3$	10.8	-	108.10	-	-
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} \text{m}^2/\text{s}]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$	
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} \text{m}^2/\text{s}]$	$[10^{-6} {\rm m}^2/{\rm s}]$	
20	398.15	0.0	1.00	$30.2 \pm 1.0$	31.9	7.29	-	-	-	
20	398.15	0.1	0.92	$26.0\pm0.6$	28.0	8.96	35.89	$0.34\pm0.01$	$0.32\pm0.01$	
20	398.15	0.2	0.86	$25.0 \pm 1.9$	25.5	10.76	44.05	$0.40\pm0.01$	$0.34\pm0.01$	
20	398.15	0.3	0.82	$23.0\pm0.5$	23.8	12.58	50.97	$0.45 \pm 0.02$	$0.37\pm0.01$	
20	398.15	0.4	0.80	$21.6 \pm 1.4$	22.5	15.00	58.52	$0.48 \pm 0.03$	$0.38\pm0.02$	
20	398.15	0.5	0.79	$20.2\pm0.8$	21.4	17.21	66.72	$0.51\pm0.02$	$0.40\pm0.02$	
20	398.15	0.6	0.81	$19.5\pm0.8$	20.4	20.48	74.56	$0.53\pm0.01$	$0.42 \pm 0.01$	
20	398.15	0.7	0.83	$18.9\pm0.8$	19.3	24.68	83.98	$0.56 \pm 0.03$	$0.47\pm0.03$	
20	398.15	0.8	0.87	$17.1\pm0.8$	17.9	30.22	95.10	$0.58\pm0.02$	$0.51\pm0.02$	
20	398.15	0.9	0.93	$15.2 \pm 1.3$	15.8	37.95	107.94	$0.56 \pm 0.01$	$0.52\pm0.01$	
20	398.15	1.0	1.00	$10.9\pm0.5$	11.2	-	121.09	-	-	
20	423.15	0.0	1.00	$29.1 \pm 1.3$	29.8	9.05	-	-	-	
20	423.15	0.1	0.95	$26.7\pm0.6$	27.3	10.83	44.04	$0.42 \pm 0.01$	$0.40\pm0.01$	
20	423.15	0.2	0.90	$24.3\pm0.2$	25.6	12.50	51.34	$0.46 \pm 0.02$	$0.41 \pm 0.02$	
20	423.15	0.3	0.87	$23.7 \pm 1.5$	24.2	14.41	59.56	$0.52\pm0.02$	$0.45\pm0.02$	
20	423.15	0.4	0.85	$22.3 \pm 1.3$	23.1	16.92	66.57	$0.54\pm0.01$	$0.46 \pm 0.01$	
20	423.15	0.5	0.84	$21.3 \pm 1.1$	22.1	19.47	74.77	$0.57\pm0.02$	$0.48\pm0.01$	
20	423.15	0.6	0.84	$20.2\pm0.6$	21.2	22.87	83.57	$0.59\pm0.02$	$0.50\pm0.02$	
20	423.15	0.7	0.86	$19.0\pm0.7$	20.1	27.35	94.49	$0.60 \pm 0.01$	$0.52\pm0.01$	
20	423.15	0.8	0.89	$17.5\pm0.9$	18.6	35.38	105.52	$0.63\pm0.03$	$0.56\pm0.03$	
20	423.15	0.9	0.94	$14.9\pm0.5$	16.4	42.40	120.56	$0.62\pm0.01$	$0.58\pm0.01$	
20	423.15	1.0	1.00	$11.1\pm0.3$	11.7	-	134.35	-	-	
25	323.15	0.0	1.00	$78.4 \pm 1.3$	77.4	2.01	-	-	-	
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta / [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
25	323.15	0.1	0.68	$52.1 \pm 0.7$	53.0	2.89	8.56	$0.09\pm0.01$	$0.06 \pm 0.01$
25	323.15	0.2	0.48	$35.5\pm0.5$	38.0	4.12	13.72	$0.14 \pm 0.01$	$0.07\pm0.01$
25	323.15	0.3	0.38	$26.8\pm0.5$	29.3	5.63	20.01	$0.19\pm0.01$	$0.07\pm0.01$
25	323.15	0.4	0.37	$22.3 \pm 0.2$	24.5	7.18	26.00	$0.24\pm0.01$	$0.09\pm0.01$
25	323.15	0.5	0.41	$19.8\pm0.6$	21.4	8.97	31.94	$0.28\pm0.01$	$0.12\pm0.01$
25	323.15	0.6	0.51	$17.7\pm0.5$	19.3	10.95	38.84	$0.30\pm0.01$	$0.15\pm0.01$
25	323.15	0.7	0.63	$16.8\pm0.5$	17.7	13.58	45.46	$0.33 \pm 0.02$	$0.21\pm0.01$
25	323.15	0.8	0.77	$15.7\pm0.7$	16.1	16.83	52.82	$0.35\pm0.04$	$0.27\pm0.03$
25	323.15	0.9	0.89	$12.9\pm0.2$	14.1	22.13	61.21	$0.35\pm0.01$	$0.31\pm0.01$
25	323.15	1.0	1.00	$9.8\pm0.4$	10.0	-	71.11	-	-
25	348.15	0.0	1.00	$57.4 \pm 0.8$	59.0	2.93	-	-	-
25	348.15	0.1	0.78	$39.9\pm0.3$	42.4	4.13	13.48	$0.14\pm0.01$	$0.11 \pm 0.01$
25	348.15	0.2	0.63	$29.6 \pm 1.1$	32.7	5.58	19.74	$0.19\pm0.01$	$0.12\pm0.01$
25	348.15	0.3	0.56	$25.1\pm0.4$	27.2	7.09	25.90	$0.24\pm0.01$	$0.13\pm0.01$
25	348.15	0.4	0.54	$21.8\pm0.7$	23.8	8.72	32.35	$0.28\pm0.01$	$0.15\pm0.01$
25	348.15	0.5	0.56	$20.3\pm0.5$	21.6	10.58	38.50	$0.32\pm0.02$	$0.18\pm0.01$
25	348.15	0.6	0.62	$20.1 \pm 4.1$	19.8	13.09	45.77	$0.36\pm0.02$	$0.23\pm0.01$
25	348.15	0.7	0.71	$17.4 \pm 0.8$	18.3	15.88	52.84	$0.37\pm0.01$	$0.26\pm0.01$
25	348.15	0.8	0.81	$15.6\pm0.5$	16.8	19.56	60.85	$0.37\pm0.01$	$0.30\pm0.01$
25	348.15	0.9	0.91	$13.4 \pm 0.4$	14.7	24.51	70.52	$0.39\pm0.01$	$0.35\pm0.01$
25	348.15	1.0	1.00	$10.2 \pm 0.3$	10.5	-	78.70	-	-
25	373.15	0.0	1.00	$43.5\pm0.5$	46.4	4.12	-	-	-
25	373.15	0.1	0.85	$33.0\pm0.5$	36.0	5.55	19.54	$0.19\pm0.01$	$0.16 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta / [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
25	373.15	0.2	0.75	$28.0\pm0.7$	30.0	7.03	26.07	$0.24 \pm 0.01$	$0.18\pm0.01$
25	373.15	0.3	0.69	$24.6\pm0.9$	26.2	8.61	32.32	$0.29\pm0.01$	$0.20\pm0.01$
25	373.15	0.4	0.66	$22.9 \pm 1.2$	23.7	10.32	38.56	$0.33\pm0.01$	$0.22\pm0.01$
25	373.15	0.5	0.67	$21.3\pm0.8$	21.9	12.41	45.52	$0.36\pm0.01$	$0.24\pm0.01$
25	373.15	0.6	0.70	$21.1 \pm 1.4$	20.4	14.91	52.24	$0.39\pm0.01$	$0.27\pm0.01$
25	373.15	0.7	0.76	$18.2\pm0.6$	19.0	17.85	59.94	$0.40\pm0.01$	$0.30\pm0.01$
25	373.15	0.8	0.83	$16.1 \pm 0.3$	17.5	21.71	68.65	$0.44\pm0.02$	$0.37\pm0.02$
25	373.15	0.9	0.91	$14.5\pm0.7$	15.3	28.27	78.06	$0.42\pm0.01$	$0.38\pm0.01$
25	373.15	1.0	1.00	$10.3\pm0.2$	10.9	-	88.49	-	-
25	398.15	0.0	1.00	$41.3 \pm 11.0$	38.9	5.54	-	-	-
25	398.15	0.1	0.90	$30.2\pm0.5$	32.5	6.97	26.03	$0.25\pm0.01$	$0.23\pm0.01$
25	398.15	0.2	0.83	$26.6\pm0.8$	28.6	8.57	32.51	$0.30\pm0.01$	$0.25\pm0.01$
25	398.15	0.3	0.78	$24.8 \pm 0.4$	25.9	10.19	38.44	$0.35\pm0.01$	$0.27 \pm 0.01$
25	398.15	0.4	0.75	$22.8 \pm 1.2$	23.9	12.00	44.97	$0.38\pm0.01$	$0.29\pm0.01$
25	398.15	0.5	0.75	$20.8\pm0.3$	22.4	14.05	51.73	$0.40\pm0.01$	$0.30\pm0.01$
25	398.15	0.6	0.76	$20.1\pm0.4$	21.1	16.56	59.48	$0.42\pm0.01$	$0.32\pm0.01$
25	398.15	0.7	0.80	$18.3\pm0.8$	19.7	20.05	66.87	$0.44 \pm 0.02$	$0.35\pm0.01$
25	398.15	0.8	0.85	$16.8\pm0.5$	18.2	24.67	76.79	$0.48\pm0.01$	$0.41\pm0.01$
25	398.15	0.9	0.92	$14.3\pm0.3$	15.9	31.13	87.44	$0.50\pm0.06$	$0.46 \pm 0.05$
25	398.15	1.0	1.00	$11.1 \pm 0.3$	11.3	-	98.55	-	-
25	423.15	0.0	1.00	$32.5\pm0.3$	34.9	7.02	-	-	-
25	423.15	0.1	0.93	$29.2\pm0.9$	30.8	8.52	32.25	$0.31\pm0.01$	$0.29\pm0.01$
25	423.15	0.2	0.88	$26.0\pm0.5$	28.0	10.06	39.12	$0.36 \pm 0.01$	$0.31 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa]$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
25	423.15	0.3	0.84	$25.6 \pm 2.1$	25.9	11.74	45.50	$0.39\pm0.01$	$0.33 \pm 0.01$
25	423.15	0.4	0.81	$23.3\pm0.6$	24.3	13.62	52.22	$0.42\pm0.01$	$0.34\pm0.01$
25	423.15	0.5	0.80	$22.2 \pm 0.6$	23.0	15.84	59.06	$0.47\pm0.01$	$0.37\pm0.01$
25	423.15	0.6	0.80	$20.6\pm0.2$	21.8	18.77	66.90	$0.49\pm0.01$	$0.39\pm0.01$
25	423.15	0.7	0.83	$19.3\pm0.7$	20.5	22.24	75.31	$0.49\pm0.01$	$0.41 \pm 0.01$
25	423.15	0.8	0.87	$17.7\pm0.6$	18.9	27.38	84.76	$0.52\pm0.03$	$0.45\pm0.02$
25	423.15	0.9	0.92	$15.0\pm0.8$	16.5	34.73	96.83	$0.52\pm0.01$	$0.48\pm0.01$
25	423.15	1.0	1.00	$11.3\pm0.5$	11.8	-	107.97	-	-
30	323.15	0.0	1.00	$86.4\pm0.7$	84.8	1.86	-	-	_
30	323.15	0.1	0.69	$60.5\pm0.2$	59.3	2.55	7.27	$0.07\pm0.01$	$0.05\pm0.01$
30	323.15	0.2	0.49	$41.7\pm0.4$	43.2	3.52	10.95	$0.11\pm0.01$	$0.06\pm0.01$
30	323.15	0.3	0.38	$30.3\pm0.4$	33.1	4.72	15.59	$0.16\pm0.01$	$0.06 \pm 0.01$
30	323.15	0.4	0.35	$25.0\pm0.6$	26.9	6.12	20.75	$0.20\pm0.01$	$0.07 \pm 0.01$
30	323.15	0.5	0.38	$21.2 \pm 0.4$	23.1	7.64	26.33	$0.23\pm0.01$	$0.09\pm0.01$
30	323.15	0.6	0.46	$20.0 \pm 1.4$	20.4	9.44	31.95	$0.26\pm0.01$	$0.12\pm0.01$
30	323.15	0.7	0.57	$17.3\pm0.6$	18.4	11.68	37.99	$0.29\pm0.02$	$0.17\pm0.01$
30	323.15	0.8	0.71	$15.2\pm0.3$	16.5	14.82	44.68	$0.29\pm0.01$	$0.20\pm0.01$
30	323.15	0.9	0.86	$12.8\pm0.4$	14.3	18.85	52.25	$0.30\pm0.01$	$0.26\pm0.01$
30	323.15	1.0	1.00	$10.3\pm0.6$	10.2	-	59.42	-	-
30	348.15	0.0	1.00	$65.7\pm0.6$	66.7	2.54	-	-	-
30	348.15	0.1	0.77	$46.1\pm0.5$	48.7	3.51	10.61	$0.11\pm0.01$	$0.08 \pm 0.01$
30	348.15	0.2	0.62	$34.8\pm0.5$	37.4	4.67	15.22	$0.15\pm0.01$	$0.09\pm0.01$
30	348.15	0.3	0.53	$27.6 \pm 1.0$	30.3	5.99	20.62	$0.20 \pm 0.01$	$0.10\pm0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu P a]$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H_2}}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
30	348.15	0.4	0.50	$24.5 \pm 1.5$	26.0	7.42	25.98	$0.24 \pm 0.01$	$0.12 \pm 0.01$
30	348.15	0.5	0.52	$22.0 \pm 1.8$	23.0	9.14	31.58	$0.26\pm0.01$	$0.14 \pm 0.01$
30	348.15	0.6	0.58	$19.5\pm0.7$	20.8	10.91	37.15	$0.28\pm0.01$	$0.16\pm0.01$
30	348.15	0.7	0.66	$17.8\pm0.6$	18.9	13.54	43.72	$0.31\pm0.01$	$0.20\pm0.01$
30	348.15	0.8	0.77	$16.3\pm0.5$	17.1	16.77	50.45	$0.32 \pm 0.01$	$0.24 \pm 0.01$
30	348.15	0.9	0.88	$14.2 \pm 1.0$	14.9	21.91	59.11	$0.32 \pm 0.01$	$0.28\pm0.01$
30	348.15	1.0	1.00	$10.3\pm0.7$	10.6	-	67.40	-	-
30	373.15	0.0	1.00	$51.4 \pm 1.3$	54.0	3.44	-	-	-
30	373.15	0.1	0.84	$38.8\pm0.8$	41.6	4.59	14.96	$0.15\pm0.01$	$0.12 \pm 0.01$
30	373.15	0.2	0.72	$31.3\pm0.7$	33.7	5.88	20.22	$0.20\pm0.01$	$0.14 \pm 0.01$
30	373.15	0.3	0.65	$27.1 \pm 1.0$	28.9	7.22	25.82	$0.23\pm0.01$	$0.15\pm0.01$
30	373.15	0.4	0.62	$24.0\pm0.3$	25.6	8.79	31.44	$0.27\pm0.01$	$0.17\pm0.01$
30	373.15	0.5	0.63	$22.3 \pm 1.2$	23.1	10.58	37.05	$0.30 \pm 0.01$	$0.19\pm0.01$
30	373.15	0.6	0.66	$21.5 \pm 2.3$	21.2	12.64	43.34	$0.33\pm0.01$	$0.22 \pm 0.01$
30	373.15	0.7	0.72	$17.0 \pm 3.2$	19.5	15.37	49.97	$0.35\pm0.01$	$0.25\pm0.01$
30	373.15	0.8	0.80	$16.6\pm0.3$	17.8	19.01	57.62	$0.36\pm0.01$	$0.29\pm0.01$
30	373.15	0.9	0.89	$15.0 \pm 1.1$	15.5	23.92	66.03	$0.36\pm0.01$	$0.32\pm0.01$
30	373.15	1.0	1.00	$10.4\pm0.5$	11.0	-	74.20	-	-
30	398.15	0.0	1.00	$42.9 \pm 1.1$	45.5	4.57	-	-	-
30	398.15	0.1	0.89	$34.4\pm0.4$	37.1	5.78	20.07	$0.20\pm0.01$	$0.17 \pm 0.01$
30	398.15	0.2	0.80	$30.3 \pm 1.3$	31.8	7.10	25.90	$0.24\pm0.01$	$0.20 \pm 0.01$
30	398.15	0.3	0.74	$26.9\pm0.6$	28.1	8.62	30.90	$0.28\pm0.01$	$0.21 \pm 0.01$
30	398.15	0.4	0.71	$24.0\pm0.4$	25.5	10.13	36.97	$0.31\pm0.01$	$0.22 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta / [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
30	398.15	0.5	0.71	$22.2 \pm 0.7$	23.5	12.02	42.73	$0.35 \pm 0.02$	$0.25\pm0.02$
30	398.15	0.6	0.72	$20.9\pm0.6$	21.8	14.31	49.35	$0.37\pm0.01$	$0.26\pm0.01$
30	398.15	0.7	0.76	$18.9\pm0.6$	20.2	17.36	56.46	$0.38\pm0.01$	$0.29\pm0.01$
30	398.15	0.8	0.82	$17.2 \pm 0.3$	18.5	21.27	64.21	$0.41 \pm 0.03$	$0.34\pm0.03$
30	398.15	0.9	0.90	$15.0\pm0.5$	16.1	27.10	74.09	$0.42\pm0.03$	$0.38\pm0.03$
30	398.15	1.0	1.00	$10.7\pm0.1$	11.4	-	83.15	-	-
30	423.15	0.0	1.00	$37.9 \pm 1.2$	40.3	5.73	-	-	-
30	423.15	0.1	0.92	$31.9 \pm 1.0$	34.6	7.00	25.47	$0.24\pm0.01$	$0.22 \pm 0.01$
30	423.15	0.2	0.85	$28.5\pm0.8$	30.6	8.35	30.68	$0.29\pm0.01$	$0.24 \pm 0.01$
30	423.15	0.3	0.81	$25.6\pm0.4$	27.8	9.84	36.51	$0.33\pm0.01$	$0.26\pm0.01$
30	423.15	0.4	0.78	$24.2\pm0.6$	25.7	11.67	42.50	$0.36\pm0.01$	$0.28\pm0.01$
30	423.15	0.5	0.76	$22.9\pm0.4$	23.9	13.77	49.00	$0.38\pm0.01$	$0.29\pm0.01$
30	423.15	0.6	0.77	$22.3 \pm 2.5$	22.4	16.08	55.20	$0.40\pm0.01$	$0.31 \pm 0.01$
30	423.15	0.7	0.80	$20.0 \pm 0.4$	20.9	19.04	63.55	$0.43 \pm 0.01$	$0.34\pm0.01$
30	423.15	0.8	0.84	$18.4 \pm 0.4$	19.2	24.32	71.16	$0.46 \pm 0.04$	$0.39\pm0.04$
30	423.15	0.9	0.91	$15.7 \pm 1.1$	16.7	29.57	81.57	$0.43 \pm 0.02$	$0.40\pm0.01$
30	423.15	1.0	1.00	$11.7\pm0.8$	11.9	-	91.97	-	-
35	323.15	0.0	1.00	$92.7 \pm 0.8$	91.3	1.73	-	-	-
35	323.15	0.1	0.70	$66.8 \pm 1.0$	64.8	2.32	6.36	$0.07\pm0.01$	$0.05\pm0.01$
35	323.15	0.2	0.50	$47.7\pm0.5$	47.7	3.15	9.27	$0.10 \pm 0.01$	$0.05\pm0.01$
35	323.15	0.3	0.38	$35.1 \pm 0.8$	36.6	4.15	13.09	$0.14\pm0.01$	$0.05 \pm 0.01$
35	323.15	0.4	0.34	$28.4 \pm 1.2$	29.4	5.38	17.37	$0.17 \pm 0.01$	$0.06 \pm 0.01$
35	323.15	0.5	0.35	$22.9 \pm 0.1$	24.7	6.75	22.23	$0.21 \pm 0.01$	$0.07 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
35	323.15	0.6	0.42	$20.0 \pm 0.4$	21.6	8.36	27.09	$0.23 \pm 0.01$	$0.10 \pm 0.01$
35	323.15	0.7	0.53	$18.1\pm0.9$	19.1	10.25	32.85	$0.24\pm0.01$	$0.13\pm0.01$
35	323.15	0.8	0.67	$15.6\pm0.3$	16.9	13.15	38.85	$0.26\pm0.01$	$0.17\pm0.01$
35	323.15	0.9	0.83	$14.4 \pm 1.1$	14.6	17.05	44.87	$0.26\pm0.01$	$0.22\pm0.01$
35	323.15	1.0	1.00	$10.2\pm0.4$	10.3	-	52.23	-	-
35	348.15	0.0	1.00	$72.3 \pm 1.2$	73.3	2.35	-	-	-
35	348.15	0.1	0.77	$52.5\pm0.5$	54.0	3.09	8.84	$0.09\pm0.01$	$0.07\pm0.01$
35	348.15	0.2	0.62	$39.0\pm0.3$	41.5	4.09	12.72	$0.13\pm0.01$	$0.08\pm0.01$
35	348.15	0.3	0.52	$34.3\pm5.6$	33.4	5.23	17.15	$0.17\pm0.01$	$0.09\pm0.01$
35	348.15	0.4	0.48	$26.3\pm0.6$	28.0	6.55	21.82	$0.20\pm0.01$	$0.10\pm0.01$
35	348.15	0.5	0.49	$23.2\pm0.6$	24.5	7.97	26.88	$0.23\pm0.01$	$0.11\pm0.01$
35	348.15	0.6	0.54	$20.6 \pm 1.2$	21.7	9.73	31.98	$0.25\pm0.01$	$0.14\pm0.01$
35	348.15	0.7	0.62	$18.4\pm0.6$	19.5	11.98	37.60	$0.27\pm0.01$	$0.17\pm0.01$
35	348.15	0.8	0.73	$16.4\pm0.5$	17.5	14.85	44.16	$0.28\pm0.01$	$0.21\pm0.01$
35	348.15	0.9	0.86	$13.9\pm0.3$	15.1	18.92	50.72	$0.29\pm0.01$	$0.25\pm0.01$
35	348.15	1.0	1.00	$10.1\pm0.1$	10.7	-	58.28	-	-
35	373.15	0.0	1.00	$59.4 \pm 0.9$	60.5	3.08	-	-	-
35	373.15	0.1	0.83	$44.2\pm0.6$	46.5	3.99	12.33	$0.12\pm0.01$	$0.10\pm0.01$
35	373.15	0.2	0.71	$35.3 \pm 1.2$	37.4	5.09	16.82	$0.16 \pm 0.01$	$0.11 \pm 0.01$
35	373.15	0.3	0.63	$29.8 \pm 1.5$	31.4	6.31	21.49	$0.20\pm0.01$	$0.13\pm0.01$
35	373.15	0.4	0.60	$25.5\pm0.6$	27.4	7.70	26.33	$0.23\pm0.01$	$0.14 \pm 0.01$
35	373.15	0.5	0.59	$23.4 \pm 1.2$	24.4	9.21	31.61	$0.26\pm0.01$	$0.16\pm0.01$
35	373.15	0.6	0.63	$20.7\pm0.7$	22.1	11.14	36.85	$0.28\pm0.01$	$0.18\pm0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
35	373.15	0.7	0.69	$19.4 \pm 0.5$	20.1	13.41	42.85	$0.30 \pm 0.01$	$0.21 \pm 0.01$
35	373.15	0.8	0.77	$15.7 \pm 1.6$	18.1	16.69	49.43	$0.32\pm0.01$	$0.24\pm0.01$
35	373.15	0.9	0.88	$14.3\pm0.3$	15.7	21.46	57.21	$0.32\pm0.01$	$0.28\pm0.01$
35	373.15	1.0	1.00	$10.5\pm0.2$	11.2	-	65.08	-	-
35	398.15	0.0	1.00	$49.2 \pm 1.5$	51.5	3.94	-	-	-
35	398.15	0.1	0.88	$39.2 \pm 1.2$	41.5	5.02	16.51	$0.16\pm0.01$	$0.14\pm0.01$
35	398.15	0.2	0.78	$32.6 \pm 1.4$	34.8	6.13	20.97	$0.20\pm0.01$	$0.16\pm0.01$
35	398.15	0.3	0.72	$28.6\pm0.2$	30.4	7.46	25.44	$0.24\pm0.01$	$0.17\pm0.01$
35	398.15	0.4	0.68	$25.2\pm0.5$	27.1	8.95	30.95	$0.27\pm0.01$	$0.18 \pm 0.01$
35	398.15	0.5	0.67	$23.7\pm0.4$	24.6	10.57	35.95	$0.34\pm0.07$	$0.23\pm0.05$
35	398.15	0.6	0.69	$23.7\pm2.9$	22.5	12.45	42.04	$0.31\pm0.01$	$0.21 \pm 0.01$
35	398.15	0.7	0.74	$19.1\pm0.4$	20.7	15.05	47.83	$0.34\pm0.01$	$0.25\pm0.01$
35	398.15	0.8	0.80	$17.8\pm0.6$	18.8	18.53	55.23	$0.34\pm0.01$	$0.27 \pm 0.01$
35	398.15	0.9	0.89	$14.5\pm0.2$	16.3	24.37	64.02	$0.36 \pm 0.03$	$0.32\pm0.03$
35	398.15	1.0	1.00	$11.1\pm0.3$	11.6	-	72.72	-	-
35	423.15	0.0	1.00	$42.3 \pm 1.1$	45.5	4.96	-	-	-
35	423.15	0.1	0.91	$36.1\pm0.9$	38.3	6.07	20.93	$0.20\pm0.01$	$0.19\pm0.01$
35	423.15	0.2	0.84	$31.2\pm0.7$	33.3	7.27	25.62	$0.24\pm0.01$	$0.20 \pm 0.01$
35	423.15	0.3	0.78	$27.6\pm0.2$	29.8	8.62	30.59	$0.28\pm0.01$	$0.22\pm0.01$
35	423.15	0.4	0.75	$26.1 \pm 1.1$	27.1	10.13	35.72	$0.31\pm0.01$	$0.23\pm0.01$
35	423.15	0.5	0.73	$23.4 \pm 0.6$	24.9	11.89	41.45	$0.33\pm0.01$	$0.24 \pm 0.01$
35	423.15	0.6	0.74	$22.0\pm0.5$	23.1	14.15	47.47	$0.35\pm0.01$	$0.26 \pm 0.01$
35	423.15	0.7	0.77	$19.6\pm0.2$	21.3	17.00	53.94	$0.38\pm0.03$	$0.29\pm0.02$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta$ / [ $\mu { m Pa}$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{ m MS}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} \text{m}^2/\text{s}]$	$[10^{-6} {\rm m}^2/{\rm s}]$
35	423.15	0.8	0.82	$18.0 \pm 0.2$	19.4	20.61	61.37	$0.38 \pm 0.01$	$0.32 \pm 0.01$
35	423.15	0.9	0.90	$15.0\pm0.1$	16.9	26.38	70.79	$0.38 \pm 0.01$	$0.35\pm0.01$
35	423.15	1.0	1.00	$11.2 \pm 0.2$	12.0	-	80.06	-	-
40	323.15	0.0	1.00	$99.6 \pm 1.2$	97.3	1.63	-	-	-
40	323.15	0.1	0.71	$72.2\pm0.7$	69.7	2.16	5.77	$0.06 \pm 0.01$	$0.04 \pm 0.01$
40	323.15	0.2	0.51	$52.0\pm0.2$	51.7	2.84	8.02	$0.09\pm0.01$	$0.04\pm0.01$
40	323.15	0.3	0.39	$38.7\pm0.3$	39.8	3.75	11.22	$0.12 \pm 0.01$	$0.05\pm0.01$
40	323.15	0.4	0.33	$30.2\pm0.2$	31.8	4.77	15.00	$0.16 \pm 0.01$	$0.05\pm0.01$
40	323.15	0.5	0.34	$24.5\pm0.9$	26.3	6.06	19.03	$0.18\pm0.01$	$0.06 \pm 0.01$
40	323.15	0.6	0.40	$21.6 \pm 1.1$	22.5	7.50	23.75	$0.21 \pm 0.01$	$0.08\pm0.01$
40	323.15	0.7	0.50	$18.4\pm0.4$	19.8	9.32	28.58	$0.22 \pm 0.01$	$0.11\pm0.01$
40	323.15	0.8	0.64	$15.9\pm0.2$	17.4	11.87	33.79	$0.23\pm0.01$	$0.15\pm0.01$
40	323.15	0.9	0.81	$13.5\pm0.1$	14.8	15.68	40.18	$0.23 \pm 0.01$	$0.19 \pm 0.01$
40	323.15	1.0	1.00	$10.1\pm0.1$	10.5	-	46.22	-	-
40	348.15	0.0	1.00	$79.4\pm0.6$	79.1	2.17	-	-	-
40	348.15	0.1	0.78	$58.7\pm0.6$	58.8	2.81	7.94	$0.08\pm0.01$	$0.06\pm0.01$
40	348.15	0.2	0.62	$44.2\pm0.5$	45.3	3.66	10.83	$0.11 \pm 0.01$	$0.07\pm0.01$
40	348.15	0.3	0.51	$34.2\pm0.5$	36.2	4.69	14.57	$0.14 \pm 0.01$	$0.07\pm0.01$
40	348.15	0.4	0.47	$28.5\pm0.6$	30.1	5.84	18.62	$0.18\pm0.01$	$0.08\pm0.01$
40	348.15	0.5	0.47	$24.7\pm0.6$	25.7	7.13	23.10	$0.20 \pm 0.01$	$0.10\pm0.01$
40	348.15	0.6	0.51	$21.1\pm0.4$	22.7	8.76	27.76	$0.23 \pm 0.01$	$0.12 \pm 0.01$
40	348.15	0.7	0.59	$19.2\pm0.5$	20.2	10.72	32.92	$0.25 \pm 0.01$	$0.15\pm0.01$
40	348.15	0.8	0.70	$16.6 \pm 0.4$	17.9	13.85	38.65	$0.25\pm0.01$	$0.17 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
40	348.15	0.9	0.84	$14.2 \pm 0.6$	15.4	17.19	45.40	$0.27\pm0.01$	$0.23 \pm 0.01$
40	348.15	1.0	1.00	$10.4\pm0.3$	10.9	-	52.01	-	-
40	373.15	0.0	1.00	$63.7\pm0.3$	66.2	2.80	-	-	-
40	373.15	0.1	0.83	$49.3\pm0.2$	51.0	3.58	10.61	$0.11 \pm 0.01$	$0.09\pm0.01$
40	373.15	0.2	0.70	$39.0\pm0.7$	40.9	4.58	14.04	$0.14 \pm 0.01$	$0.10\pm0.01$
40	373.15	0.3	0.62	$32.1\pm0.2$	33.9	5.66	18.23	$0.18\pm0.01$	$0.11 \pm 0.01$
40	373.15	0.4	0.58	$28.0\pm0.4$	29.0	6.86	22.52	$0.20\pm0.01$	$0.12\pm0.01$
40	373.15	0.5	0.57	$23.9\pm0.5$	25.7	8.30	27.54	$0.23\pm0.01$	$0.13\pm0.01$
40	373.15	0.6	0.60	$21.7\pm0.8$	23.0	9.95	32.08	$0.25\pm0.01$	$0.15\pm0.01$
40	373.15	0.7	0.66	$19.1\pm0.5$	20.7	12.38	37.44	$0.27\pm0.01$	$0.18\pm0.01$
40	373.15	0.8	0.75	$17.5\pm0.3$	18.5	14.97	43.55	$0.28\pm0.01$	$0.21\pm0.01$
40	373.15	0.9	0.86	$14.5\pm0.7$	15.9	19.55	50.88	$0.29\pm0.01$	$0.25\pm0.01$
40	373.15	1.0	1.00	$10.7\pm0.2$	11.3	-	57.53	-	-
40	398.15	0.0	1.00	$54.2\pm0.8$	56.9	3.56	-	-	-
40	398.15	0.1	0.87	$43.0\pm0.6$	45.6	4.47	13.92	$0.14 \pm 0.01$	$0.12\pm0.01$
40	398.15	0.2	0.77	$35.6\pm0.5$	37.9	5.50	17.71	$0.17\pm0.01$	$0.13\pm0.01$
40	398.15	0.3	0.70	$30.7\pm0.6$	32.4	6.61	22.15	$0.21 \pm 0.01$	$0.14 \pm 0.01$
40	398.15	0.4	0.66	$26.6\pm0.4$	28.7	8.00	26.72	$0.23\pm0.01$	$0.15\pm0.01$
40	398.15	0.5	0.65	$24.6\pm0.5$	25.7	9.44	31.58	$0.26 \pm 0.01$	$0.17\pm0.01$
40	398.15	0.6	0.67	$21.6\pm0.4$	23.3	11.33	36.82	$0.28\pm0.01$	$0.18\pm0.01$
40	398.15	0.7	0.71	$20.0\pm0.3$	21.2	13.64	42.44	$0.30\pm0.01$	$0.21 \pm 0.01$
40	398.15	0.8	0.78	$17.5\pm0.4$	19.1	16.77	48.52	$0.31 \pm 0.01$	$0.24 \pm 0.01$
40	398.15	0.9	0.88	$15.5 \pm 1.5$	16.5	21.24	56.52	$0.33 \pm 0.01$	$0.29 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta / [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} \text{m}^2/\text{s}]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
40	398.15	1.0	1.00	$11.1 \pm 0.1$	11.7	-	64.00	-	-
40	423.15	0.0	1.00	$46.8\pm0.6$	50.3	4.38	-	-	-
40	423.15	0.1	0.90	$39.6 \pm 1.4$	41.9	5.35	17.42	$0.17\pm0.01$	$0.15\pm0.01$
40	423.15	0.2	0.82	$34.7 \pm 2.1$	35.9	6.45	21.57	$0.21\pm0.01$	$0.17\pm0.01$
40	423.15	0.3	0.76	$30.0 \pm 0.8$	31.7	7.63	26.13	$0.24 \pm 0.01$	$0.18\pm0.01$
40	423.15	0.4	0.73	$27.0\pm0.8$	28.5	9.05	30.92	$0.27\pm0.01$	$0.19\pm0.01$
40	423.15	0.5	0.71	$24.4 \pm 1.0$	25.9	10.62	36.00	$0.29\pm0.01$	$0.21\pm0.01$
40	423.15	0.6	0.72	$22.4 \pm 0.3$	23.8	12.66	41.39	$0.31\pm0.01$	$0.22 \pm 0.01$
40	423.15	0.7	0.75	$20.4 \pm 0.4$	21.8	15.14	47.69	$0.32\pm0.01$	$0.24\pm0.01$
40	423.15	0.8	0.81	$18.2\pm0.3$	19.7	18.51	54.32	$0.34\pm0.01$	$0.27\pm0.01$
40	423.15	0.9	0.89	$16.1 \pm 1.4$	17.1	23.32	62.34	$0.35\pm0.01$	$0.31\pm0.01$
40	423.15	1.0	1.00	$11.7\pm0.7$	12.1	-	70.81	-	-
45	323.15	0.0	1.00	$106.0 \pm 1.2$	102.9	1.56	-	-	-
45	323.15	0.1	0.72	$77.0\pm0.5$	74.3	2.01	5.29	$0.05\pm0.01$	$0.04\pm0.01$
45	323.15	0.2	0.52	$57.7 \pm 1.7$	55.4	2.67	7.33	$0.08\pm0.01$	$0.04\pm0.01$
45	323.15	0.3	0.39	$42.5\pm0.3$	42.7	3.45	9.97	$0.11 \pm 0.01$	$0.04 \pm 0.01$
45	323.15	0.4	0.33	$32.7\pm0.4$	34.0	4.40	13.36	$0.14\pm0.01$	$0.05\pm0.01$
45	323.15	0.5	0.32	$26.2 \pm 0.3$	27.9	5.50	16.91	$0.17\pm0.01$	$0.05\pm0.01$
45	323.15	0.6	0.37	$21.9\pm0.4$	23.6	6.92	20.82	$0.19\pm0.01$	$0.07\pm0.01$
45	323.15	0.7	0.47	$19.0\pm0.1$	20.4	8.54	25.43	$0.21\pm0.01$	$0.10\pm0.01$
45	323.15	0.8	0.61	$17.0\pm0.6$	17.8	10.89	30.62	$0.21\pm0.01$	$0.13\pm0.01$
45	323.15	0.9	0.79	$13.7\pm0.5$	15.1	14.12	36.20	$0.21 \pm 0.01$	$0.17\pm0.01$
45	323.15	1.0	1.00	$10.2\pm0.1$	10.6	-	41.86	_	-
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa]$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
45	348.15	0.0	1.00	$86.1 \pm 1.2$	84.5	2.02	-	-	-
45	348.15	0.1	0.78	$63.3\pm0.9$	63.1	2.60	7.14	$0.07\pm0.01$	$0.06\pm0.01$
45	348.15	0.2	0.62	$48.4\pm0.6$	48.7	3.35	9.69	$0.10\pm0.01$	$0.06\pm0.01$
45	348.15	0.3	0.51	$38.3 \pm 1.9$	38.9	4.26	12.83	$0.13\pm0.01$	$0.06\pm0.01$
45	348.15	0.4	0.45	$30.4\pm0.2$	32.0	5.33	16.38	$0.16 \pm 0.01$	$0.07\pm0.01$
45	348.15	0.5	0.45	$25.4 \pm 0.4$	27.1	6.53	20.29	$0.19\pm0.01$	$0.08\pm0.01$
45	348.15	0.6	0.49	$22.1 \pm 0.4$	23.5	8.01	24.75	$0.21 \pm 0.01$	$0.10\pm0.01$
45	348.15	0.7	0.56	$19.5\pm0.8$	20.8	9.85	29.55	$0.22\pm0.01$	$0.12\pm0.01$
45	348.15	0.8	0.68	$17.1 \pm 0.4$	18.3	12.34	34.71	$0.23\pm0.01$	$0.16 \pm 0.01$
45	348.15	0.9	0.82	$14.3\pm0.2$	15.6	15.64	40.76	$0.25\pm0.01$	$0.20\pm0.01$
45	348.15	1.0	1.00	$10.8\pm0.4$	11.0	-	47.17	-	-
45	373.15	0.0	1.00	$70.1\pm0.7$	71.3	2.58	-	-	-
45	373.15	0.1	0.83	$53.7\pm0.5$	55.1	3.29	9.48	$0.10\pm0.01$	$0.08\pm0.01$
45	373.15	0.2	0.70	$42.3\pm0.6$	44.0	4.14	12.41	$0.12 \pm 0.01$	$0.09\pm0.01$
45	373.15	0.3	0.61	$34.5\pm0.4$	36.3	5.16	16.10	$0.15\pm0.01$	$0.09\pm0.01$
45	373.15	0.4	0.56	$29.0\pm0.1$	30.8	6.23	19.78	$0.19\pm0.01$	$0.11 \pm 0.01$
45	373.15	0.5	0.55	$24.9\pm0.4$	26.8	7.62	24.15	$0.20\pm0.01$	$0.11 \pm 0.01$
45	373.15	0.6	0.57	$22.7\pm0.5$	23.8	9.06	28.53	$0.23\pm0.01$	$0.13\pm0.01$
45	373.15	0.7	0.63	$19.7\pm0.3$	21.2	11.03	33.26	$0.25\pm0.01$	$0.16\pm0.01$
45	373.15	0.8	0.73	$17.6\pm0.9$	18.8	13.73	39.31	$0.26 \pm 0.01$	$0.19\pm0.01$
45	373.15	0.9	0.85	$14.9\pm0.8$	16.1	17.57	45.52	$0.27\pm0.01$	$0.23 \pm 0.01$
45	373.15	1.0	1.00	$10.7\pm0.3$	11.4	-	52.40	-	-
45	398.15	0.0	1.00	$59.4\pm0.7$	61.7	3.24	_	-	-
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta / [\mu Pa$	as]	$D^{\text{self}}$ /	$[10^{-8} \text{m}^2/\text{s}]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
45	398.15	0.1	0.87	$47.0 \pm 0.6$	49.3	4.05	12.26	$0.12 \pm 0.01$	$0.10 \pm 0.01$
45	398.15	0.2	0.76	$38.4 \pm 0.5$	40.7	4.98	15.57	$0.15\pm0.01$	$0.12\pm0.01$
45	398.15	0.3	0.69	$33.5\pm0.9$	34.6	5.99	19.45	$0.18\pm0.01$	$0.12\pm0.01$
45	398.15	0.4	0.64	$28.6\pm0.5$	30.1	7.23	23.32	$0.21\pm0.01$	$0.13\pm0.01$
45	398.15	0.5	0.63	$25.0\pm0.6$	26.8	8.60	27.95	$0.24\pm0.01$	$0.15 \pm 0.01$
45	398.15	0.6	0.64	$22.8\pm0.7$	24.1	10.35	32.55	$0.26\pm0.01$	$0.17\pm0.01$
45	398.15	0.7	0.69	$20.9\pm0.8$	21.7	12.32	37.67	$0.27\pm0.01$	$0.18\pm0.01$
45	398.15	0.8	0.76	$18.4\pm0.7$	19.4	15.25	43.90	$0.29\pm0.02$	$0.22 \pm 0.01$
45	398.15	0.9	0.87	$15.7\pm0.8$	16.7	19.79	50.68	$0.29\pm0.01$	$0.25 \pm 0.01$
45	398.15	1.0	1.00	$11.1 \pm 0.1$	11.8	-	58.25	-	-
45	423.15	0.0	1.00	$51.7 \pm 0.5$	54.8	3.99	-	-	-
45	423.15	0.1	0.90	$44.0 \pm 1.6$	45.3	4.81	15.08	$0.15\pm0.01$	$0.13 \pm 0.01$
45	423.15	0.2	0.81	$36.2 \pm 0.4$	38.5	5.80	18.73	$0.18\pm0.01$	$0.15 \pm 0.01$
45	423.15	0.3	0.75	$31.7 \pm 0.5$	33.5	6.93	22.95	$0.21\pm0.01$	$0.16\pm0.01$
45	423.15	0.4	0.71	$29.9 \pm 4.2$	29.9	8.17	27.00	$0.24\pm0.01$	$0.17\pm0.01$
45	423.15	0.5	0.69	$26.0\pm0.9$	27.0	9.76	31.82	$0.26 \pm 0.01$	$0.18\pm0.01$
45	423.15	0.6	0.70	$22.8 \pm 0.4$	24.5	11.51	36.60	$0.28\pm0.01$	$0.19 \pm 0.01$
45	423.15	0.7	0.73	$20.8 \pm 1.2$	22.3	13.77	41.91	$0.29\pm0.01$	$0.21 \pm 0.01$
45	423.15	0.8	0.79	$18.3\pm0.2$	20.0	16.97	48.92	$0.32 \pm 0.01$	$0.25\pm0.01$
45	423.15	0.9	0.88	$15.7\pm0.2$	17.3	21.67	55.98	$0.32 \pm 0.01$	$0.28\pm0.01$
45	423.15	1.0	1.00	$11.7\pm0.3$	12.2	-	64.12	-	-
50	323.15	0.0	1.00	$111.1 \pm 1.3$	108.3	1.48	-	-	-
50	323.15	0.1	0.73	$82.8 \pm 1.0$	78.6	1.92	4.93	$0.05 \pm 0.01$	$0.04 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu P \epsilon]$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H_2}}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
50	323.15	0.2	0.52	$61.5\pm0.6$	58.8	2.46	6.70	$0.07\pm0.01$	$0.04 \pm 0.01$
50	323.15	0.3	0.39	$46.0\pm0.6$	45.4	3.20	9.01	$0.10\pm0.01$	$0.04\pm0.01$
50	323.15	0.4	0.32	$35.0\pm0.4$	36.1	4.08	11.97	$0.13\pm0.01$	$0.04\pm0.01$
50	323.15	0.5	0.31	$28.1\pm0.5$	29.5	5.10	15.22	$0.16\pm0.01$	$0.05\pm0.01$
50	323.15	0.6	0.35	$23.7 \pm 1.1$	24.7	6.38	18.95	$0.18\pm0.01$	$0.06 \pm 0.01$
50	323.15	0.7	0.45	$19.9\pm0.5$	21.1	7.92	22.88	$0.19\pm0.01$	$0.08\pm0.01$
50	323.15	0.8	0.59	$17.1\pm0.2$	18.2	10.07	27.64	$0.20\pm0.01$	$0.12\pm0.01$
50	323.15	0.9	0.78	$13.7\pm0.6$	15.3	12.91	32.79	$0.20\pm0.01$	$0.16\pm0.01$
50	323.15	1.0	1.00	$10.4\pm0.1$	10.8	-	38.29	-	-
50	348.15	0.0	1.00	$90.4 \pm 1.0$	89.5	1.94	-	-	-
50	348.15	0.1	0.78	$68.5\pm0.8$	67.1	2.44	6.56	$0.07\pm0.01$	$0.05\pm0.01$
50	348.15	0.2	0.62	$51.9 \pm 1.2$	51.9	3.12	8.78	$0.09\pm0.01$	$0.06\pm0.01$
50	348.15	0.3	0.50	$40.3\pm0.8$	41.4	3.96	11.55	$0.12\pm0.01$	$0.06 \pm 0.01$
50	348.15	0.4	0.44	$32.3\pm0.2$	34.0	4.90	14.80	$0.14\pm0.01$	$0.06\pm0.01$
50	348.15	0.5	0.43	$27.5 \pm 1.4$	28.5	6.01	18.27	$0.18\pm0.01$	$0.08\pm0.01$
50	348.15	0.6	0.47	$23.5 \pm 1.2$	24.5	7.37	22.14	$0.19\pm0.01$	$0.09\pm0.01$
50	348.15	0.7	0.54	$20.0\pm0.5$	21.3	9.16	26.63	$0.21\pm0.01$	$0.12 \pm 0.01$
50	348.15	0.8	0.66	$17.5\pm0.5$	18.7	11.47	31.72	$0.22\pm0.01$	$0.14\pm0.01$
50	348.15	0.9	0.81	$14.5\pm0.4$	15.8	14.77	37.29	$0.23\pm0.01$	$0.19\pm0.01$
50	348.15	1.0	1.00	$10.7\pm0.1$	11.2	-	42.80	-	-
50	373.15	0.0	1.00	$74.9\pm0.8$	76.1	2.45	-	-	_
50	373.15	0.1	0.83	$58.0\pm0.7$	58.9	3.08	8.63	$0.09\pm0.01$	$0.07\pm0.01$
50	373.15	0.2	0.69	$45.4\pm0.4$	47.0	3.84	11.09	$0.11\pm0.01$	$0.08\pm0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu Pa]$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} m^2/s]$	$[10^{-6} {\rm m}^2/{\rm s}]$
50	373.15	0.3	0.60	$37.2 \pm 0.8$	38.6	4.72	14.24	$0.14 \pm 0.01$	$0.08 \pm 0.01$
50	373.15	0.4	0.54	$31.2\pm0.6$	32.5	5.73	17.70	$0.17\pm0.01$	$0.09\pm0.01$
50	373.15	0.5	0.53	$26.3\pm0.3$	28.0	7.01	21.60	$0.19\pm0.01$	$0.10\pm0.01$
50	373.15	0.6	0.55	$22.9\pm0.5$	24.5	8.41	25.60	$0.21\pm0.01$	$0.12\pm0.01$
50	373.15	0.7	0.61	$21.2 \pm 0.8$	21.8	10.26	30.47	$0.23\pm0.01$	$0.14 \pm 0.01$
50	373.15	0.8	0.71	$17.7\pm0.3$	19.2	12.79	35.65	$0.24\pm0.01$	$0.17\pm0.01$
50	373.15	0.9	0.84	$16.1 \pm 1.4$	16.4	16.06	41.70	$0.25\pm0.01$	$0.21\pm0.01$
50	373.15	1.0	1.00	$11.1\pm0.1$	11.6	-	48.04	-	-
50	398.15	0.0	1.00	$64.1 \pm 1.1$	66.2	3.02	-	-	-
50	398.15	0.1	0.86	$50.9\pm0.5$	52.9	3.72	10.91	$0.11\pm0.01$	$0.09\pm0.01$
50	398.15	0.2	0.75	$41.5\pm0.6$	43.5	4.56	13.79	$0.13\pm0.01$	$0.10\pm0.01$
50	398.15	0.3	0.67	$34.5 \pm 1.6$	36.7	5.52	17.04	$0.16\pm0.01$	$0.11\pm0.01$
50	398.15	0.4	0.63	$30.0\pm0.5$	31.6	6.62	20.88	$0.19\pm0.01$	$0.12 \pm 0.01$
50	398.15	0.5	0.61	$26.6\pm0.8$	27.8	7.94	24.94	$0.21\pm0.01$	$0.13\pm0.01$
50	398.15	0.6	0.62	$23.1\pm0.3$	24.9	9.52	29.53	$0.23\pm0.01$	$0.15\pm0.01$
50	398.15	0.7	0.67	$20.3\pm0.7$	22.3	11.55	34.30	$0.26 \pm 0.01$	$0.17\pm0.01$
50	398.15	0.8	0.75	$18.3\pm0.1$	19.8	14.14	39.61	$0.26\pm0.01$	$0.20 \pm 0.01$
50	398.15	0.9	0.86	$16.3\pm0.6$	16.9	17.75	46.00	$0.26\pm0.01$	$0.23\pm0.01$
50	398.15	1.0	1.00	$11.6\pm0.2$	11.9	-	53.02	-	-
50	423.15	0.0	1.00	$57.3\pm0.5$	59.0	3.64	-	-	-
50	423.15	0.1	0.89	$45.8\pm0.5$	48.5	4.45	13.54	$0.13\pm0.01$	$0.12 \pm 0.01$
50	423.15	0.2	0.80	$39.0\pm0.9$	40.9	5.35	16.68	$0.16 \pm 0.01$	$0.13 \pm 0.01$
50	423.15	0.3	0.73	$33.7\pm0.6$	35.4	6.39	20.24	$0.19\pm0.01$	$0.14 \pm 0.01$
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p	Т	$x_{\mathrm{H}_2}$	$\Gamma^{\rm RFP}$	$\eta \ / \ [\mu P \epsilon$	as]	$D^{\text{self}}$ /	$[10^{-8} m^2/s]$	$D^{\mathrm{MS}}$	$D^{\mathrm{Fick}}$
[MPa]	[K]			$\eta^{ m MD}$	$\eta^{\rm RFP}$	$D_{\rm CO_2}^{\rm self}$	$D_{\mathrm{H}_2}^{\mathrm{self}}$	$[10^{-6} \text{m}^2/\text{s}]$	$[10^{-6} m^2/s]$
50	423.15	0.4	0.69	$29.9\pm0.5$	31.1	7.56	24.18	$0.22 \pm 0.01$	$0.15\pm0.01$
50	423.15	0.5	0.67	$26.9\pm0.7$	28.0	8.93	28.63	$0.24 \pm 0.01$	$0.16\pm0.01$
50	423.15	0.6	0.68	$23.9 \pm 1.0$	25.2	10.64	33.01	$0.26 \pm 0.01$	$0.18\pm0.01$
50	423.15	0.7	0.71	$24.8\pm 6.0$	22.8	12.79	38.12	$0.27\pm0.01$	$0.19\pm0.01$
50	423.15	0.8	0.78	$18.8\pm0.6$	20.3	15.64	44.13	$0.29\pm0.01$	$0.22 \pm 0.01$
50	423.15	0.9	0.87	$16.2 \pm 0.7$	17.4	19.87	50.83	$0.30 \pm 0.01$	$0.26\pm0.01$
50	423.15	1.0	1.00	$12.1 \pm 0.2$	12.3	-	58.14	-	-

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## S10.3 Phase equilibria for CO<sub>2</sub>-NaCl brine, H<sub>2</sub>-NaCl brine, and

CO<sub>2</sub>-H<sub>2</sub>-NaCl systems

Table S4: Phase equilibria for CO<sub>2</sub>-NaCl brine systems from CFCMC simulations<sup>24–26</sup> for various pressures, temperatures, and NaCl concentrations ( $c_{\text{NaCl}}$  in units of mol NaCl/kg H<sub>2</sub>O). Solubilities of CO<sub>2</sub> in the liquid-rich phase are denoted by  $x_{\text{CO}_2}$ , the water content in the gas-rich phase is denoted by  $y_{\text{H}_2\text{O}}$ , and the fugacity coefficients ( $\phi$ ) of the two species in the gas-rich phase are compared to the corresponding values from REFPROP (RFP)<sup>3</sup>. Fugacity coefficients from REFPROP for CO<sub>2</sub> and H<sub>2</sub>O at a given pressure, and temperature are obtained at the gas-phase composition obtained from CFCMC simulations.

p	Т	$c_{ m NaCl}$	$x_{\rm CO_2}$ / [10 <sup>-4</sup> ]	$y_{\rm H_{2O}} / [10^{-4}]$	$\phi_{\rm CO_2}$		$\phi_{\mathrm{H_{2}O}}$	
[MPa]	[K]				CFCMC	RFP	CFCMC	RFP
5	323.15	0	$102 \pm 7$	$32 \pm 3$	$0.81 \pm 0.01$	0.82	$0.74 \pm 0.01$	0.60
5	423.15	0	$63 \pm 2$	$1294 \pm 7$	$0.94 \pm 0.00$	0.93	$0.76 \pm 0.00$	0.81
10	323.15	0	$156 \pm 7$	$30 \pm 4$	$0.65 \pm 0.01$	0.64	$0.49 \pm 0.01$	0.26
10	423.15	0	$126 \pm 3$	$745 \pm 10$	$0.88 \pm 0.00$	0.87	$0.68 \pm 0.00$	0.67
30	323.15	0	$186 \pm 5$	$39 \pm 6$	$0.34 \pm 0.00$	0.33	$0.14 \pm 0.00$	0.09
30	423.15	0	$270 \pm 4$	$458 \pm 15$	$0.71 \pm 0.00$	0.69	$0.41 \pm 0.00$	0.36
50	323.15	0	$206 \pm 12$	$33 \pm 5$	$0.30 \pm 0.00$	0.29	$0.10 \pm 0.00$	0.08
50	423.15	0	$345 \pm 10$	$428 \pm 18$	$0.66 \pm 0.00$	0.63	$0.29 \pm 0.01$	0.29
5	323.15	1	$79 \pm 5$	$31 \pm 4$	$0.82 \pm 0.01$	0.82	$0.75 \pm 0.01$	0.60
5	423.15	1	$53 \pm 2$	$1246 \pm 7$	$0.93 \pm 0.00$	0.93	$0.76 \pm 0.00$	0.81
10	323.15	1	$126 \pm 14$	$31 \pm 6$	$0.66 \pm 0.01$	0.64	$0.49 \pm 0.01$	0.26
10	423.15	1	$102 \pm 3$	$707 \pm 10$	$0.88 \pm 0.00$	0.87	$0.69 \pm 0.00$	0.67
30	323.15	1	$145 \pm 9$	$27 \pm 5$	$0.34 \pm 0.00$	0.33	$0.14 \pm 0.00$	0.09
30	423.15	1	$218\pm9$	$438 \pm 19$	$0.71 \pm 0.00$	0.69	$0.41 \pm 0.00$	0.36
50	323.15	1	$166 \pm 4$	$34 \pm 3$	$0.29 \pm 0.00$	0.29	$0.10 \pm 0.00$	0.08
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p	Т	$c_{\rm NaCl}$	$x_{\rm CO_2} \ / \ [10^{-4}]$	$y_{\rm H_{2O}} / [10^{-4}]$	$\phi_{\rm CO_2}$		$\phi_{ m H_2O}$	
[MPa]	[K]				CFCMC	RFP	CFCMC	RFP
50	423.15	1	$270\pm8$	$400 \pm 21$	$0.66 \pm 0.00$	0.63	$0.30 \pm 0.00$	0.29
5	323.15	2	$67 \pm 5$	$31 \pm 3$	$0.83 \pm 0.00$	0.82	$0.76 \pm 0.00$	0.60
5	423.15	2	$41 \pm 2$	$1197\pm6$	$0.94 \pm 0.00$	0.93	$0.77 \pm 0.00$	0.81
10	323.15	2	$95 \pm 8$	$24 \pm 4$	$0.65 \pm 0.01$	0.64	$0.50 \pm 0.01$	0.26
10	423.15	2	$83 \pm 4$	$675 \pm 9$	$0.87 \pm 0.00$	0.87	$0.69 \pm 0.00$	0.67
30	323.15	2	$117 \pm 7$	$34 \pm 7$	$0.34 \pm 0.00$	0.33	$0.15 \pm 0.00$	0.09
30	423.15	2	$175 \pm 7$	$406\pm5$	$0.71 \pm 0.01$	0.69	$0.42 \pm 0.01$	0.36
50	323.15	2	$129 \pm 7$	$33 \pm 6$	$0.29 \pm 0.00$	0.29	$0.10 \pm 0.00$	0.08
50	423.15	2	$218 \pm 6$	$384 \pm 16$	$0.66 \pm 0.00$	0.63	$0.31 \pm 0.00$	0.29

Table S5: Phase equilibria for H<sub>2</sub>-NaCl brine systems from CFCMC simulations<sup>24–26</sup> for various pressures, temperatures, and NaCl concentrations ( $c_{\text{NaCl}}$  in units of mol NaCl/kg H<sub>2</sub>O). Solubilities of H<sub>2</sub> in the liquid-rich phase is denoted by  $x_{\text{H}_2}$ , the water content in the gas-rich phase is denoted by  $y_{\text{H}_2\text{O}}$ , and the fugacity coefficients ( $\phi$ ) of the two species in the gas-rich phase are compared to the corresponding values from REFPROP (RFP)<sup>3</sup>. Fugacity coefficients from REFPROP for H<sub>2</sub> and H<sub>2</sub>O at a given pressure, and temperature are obtained at the gas-phase composition obtained from CFCMC simulations.

p	Т	$c_{\rm NaCl}$	$x_{\rm H_2} / [10^{-4}]$	$y_{\rm H_{2O}} / [10^{-4}]$	$\phi_{\mathrm{H}_2}$		$\phi_{\mathrm{H_2O}}$	
[MPa]	[K]				CFCMC	RFP	CFCMC	RFP
5	323.15	0	$7\pm2$	$26 \pm 4$	$1.02 \pm 0.01$	1.03	$0.97\pm0.01$	0.96
5	423.15	0	$11 \pm 0$	$1185 \pm 11$	$1.02 \pm 0.00$	1.02	$0.83 \pm 0.00$	0.96
10	323.15	0	$13 \pm 2$	$12 \pm 2$	$1.04 \pm 0.01$	1.06	$0.97\pm0.01$	0.92
10	423.15	0	$24 \pm 1$	$609 \pm 15$	$1.04 \pm 0.00$	1.05	$0.84 \pm 0.00$	0.95
30	323.15	0	$42 \pm 5$	$4 \pm 1$	$1.17 \pm 0.01$	1.19	$1.01 \pm 0.01$	0.85
30	423.15	0	$71 \pm 3$	$213\pm6$	$1.14 \pm 0.01$	1.15	$0.89 \pm 0.01$	0.94
50	323.15	0	$60 \pm 6$	$3 \pm 1$	$1.31 \pm 0.00$	1.34	$1.08 \pm 0.00$	0.85
50	423.15	0	$113 \pm 5$	$134 \pm 9$	$1.24 \pm 0.01$	1.26	$0.95 \pm 0.01$	0.98
5	323.15	1	$6 \pm 1$	$25 \pm 5$	$1.01 \pm 0.01$	1.03	$0.96 \pm 0.01$	0.96
5	423.15	1	$10 \pm 1$	$1149 \pm 5$	$1.02 \pm 0.00$	1.02	$0.84 \pm 0.00$	0.96
10	323.15	1	$12 \pm 2$	$15 \pm 2$	$1.05 \pm 0.02$	1.06	$0.98 \pm 0.02$	0.92
10	423.15	1	$20 \pm 1$	$580\pm7$	$1.04 \pm 0.01$	1.05	$0.84 \pm 0.00$	0.95
30	323.15	1	$33 \pm 3$	$5 \pm 1$	$1.16 \pm 0.01$	1.19	$1.01 \pm 0.00$	0.85
30	423.15	1	$62 \pm 1$	$202\pm6$	$1.14 \pm 0.01$	1.15	$0.90 \pm 0.00$	0.94
50	323.15	1	$54 \pm 2$	$3 \pm 1$	$1.30 \pm 0.00$	1.34	$1.07 \pm 0.00$	0.85
50	423.15	1	$96 \pm 3$	$133 \pm 3$	$1.24 \pm 0.01$	1.26	$0.95 \pm 0.00$	0.98
5	323.15	2	$5\pm1$	$21 \pm 2$	$1.02 \pm 0.01$	1.03	$0.97 \pm 0.01$	0.96
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p	Т	$c_{ m NaCl}$	$x_{\rm H_2} / [10^{-4}]$	$y_{\rm H_{2O}} / [10^{-4}]$	] $\phi_{\mathrm{H}_2}$		$\phi_{\mathrm{H_2O}}$	
[MPa]	[K]				CFCMC	RFP	CFCMC	RFP
5	423.15	2	$9 \pm 1$	$1095 \pm 12$	$1.02 \pm 0.00$	1.02	$0.84 \pm 0.00$	0.96
10	323.15	2	$9\pm 2$	$14 \pm 3$	$1.05 \pm 0.00$	1.06	$0.98 \pm 0.00$	0.92
10	423.15	2	$18 \pm 1$	$561 \pm 5$	$1.04 \pm 0.00$	1.05	$0.85 \pm 0.00$	0.95
30	323.15	2	$28 \pm 3$	$5\pm 2$	$1.17 \pm 0.01$	1.19	$1.02 \pm 0.01$	0.85
30	423.15	2	$55 \pm 3$	$197\pm7$	$1.14 \pm 0.00$	1.15	$0.90 \pm 0.00$	0.95
50	323.15	2	$47 \pm 6$	$2\pm3$	$1.30 \pm 0.01$	1.34	$1.08 \pm 0.01$	0.85
50	423.15	2	$81 \pm 2$	$125 \pm 4$	$1.25 \pm 0.01$	1.26	$0.97 \pm 0.00$	0.98

p [MPa]	T [K]	$c_{\rm NaCl}$	$x_{\rm H_2} / [10^{-4}]$	$x_{\rm CO_2}$ / [10 <sup>-4</sup> ]	$y_{\rm H_2}$ / [10 <sup>-4</sup> ]	$y_{\rm H_{2O}} / [10^{-4}]$
5	323.15	0	$49 \pm 9$	$4 \pm 1$	$5029 \pm 8$	$33 \pm 4$
5	348.15	0	$43 \pm 3$	$3\pm 0$	$4997 \pm 4$	$86 \pm 8$
5	373.15	0	$34 \pm 2$	$4 \pm 0$	$4906 \pm 3$	$246 \pm 9$
5	398.15	0	$33 \pm 1$	$5\pm 0$	$4726 \pm 7$	$601 \pm 13$
5	423.15	0	$34 \pm 2$	$6 \pm 1$	$4394 \pm 5$	$1258 \pm 9$
10	323.15	0	$89\pm7$	$7\pm0$	$5074 \pm 8$	$20 \pm 3$
10	348.15	0	$73 \pm 7$	$9 \pm 1$	$5038 \pm 10$	$54 \pm 8$
10	373.15	0	$63 \pm 2$	$9\pm3$	$4983 \pm 8$	$143 \pm 11$
10	398.15	0	$60 \pm 4$	$11 \pm 1$	$4882 \pm 13$	$333 \pm 21$
10	423.15	0	$64 \pm 2$	$13 \pm 1$ $4702 \pm 10$		$690 \pm 23$
30	323.15	0	$138 \pm 8$	$23 \pm 4$	$5115 \pm 9$	$13 \pm 5$
30	348.15	0	$135 \pm 10$	$28 \pm 4$	$5097 \pm 10$	$31 \pm 4$
30	373.15	0	$133 \pm 5$	$30 \pm 5$	$5072 \pm 10$	$70 \pm 9$
30	398.15	0	$132 \pm 8$	$35 \pm 2$	$5021 \pm 7$	$158 \pm 3$
30	423.15	0	$140 \pm 3$	$44 \pm 4$	$4942 \pm 10$	$309 \pm 19$
50	323.15	0	$143 \pm 8$	$49 \pm 2$	$5092 \pm 9$	$16 \pm 2$
50	348.15	0	$149 \pm 3$	$46 \pm 2$	$5093 \pm 6$	$32 \pm 5$
50	373.15	0	$154 \pm 7$	$51 \pm 2$	$5078 \pm 13$	$62 \pm 11$
50	398.15	0	$164 \pm 4$	$59 \pm 4$	$5044 \pm 5$	$134 \pm 8$
50	423.15	0	$188 \pm 5$	$73 \pm 4$	$4996 \pm 6$	$249 \pm 7$
			Continued	l on next page		

Table S6: Phase equilibria for H<sub>2</sub>-CO<sub>2</sub>-NaCl brine systems from CFCMC simulations<sup>24–26</sup> for various pressures, temperatures, and NaCl concentrations ( $c_{\text{NaCl}}$  in units of mol NaCl/kg H<sub>2</sub>O). Solubilities of H<sub>2</sub> and CO<sub>2</sub> in the liquid-rich phase are denoted by  $x_{\text{H}_2}$  and  $x_{\text{CO}_2}$ , respectively, and the water content in the gas-rich phase is denoted by  $y_{\text{H}_2\text{O}}$ .

p [MPa]	T [K]	$c_{\rm NaCl}$	$x_{\rm H_2} / [10^{-4}]$	$x_{\rm CO_2}$ / [10 <sup>-4</sup> ]	$y_{\rm H_2} \ / \ [10^{-4}]$	$y_{\rm H_{2}O} \ / \ [10^{-4}]$
5	323.15	1	$42 \pm 4$	$3 \pm 1$	$5023 \pm 4$	$32 \pm 5$
5	348.15	1	$33 \pm 4$	$3 \pm 1$	$4982\pm6$	$96 \pm 7$
5	373.15	1	$29 \pm 3$	$4 \pm 1$	$4905\pm2$	$237\pm5$
5	398.15	1	$27 \pm 1$	$5\pm1$	$4736\pm6$	$570 \pm 12$
5	423.15	1	$26 \pm 0$	$5\pm1$	$4417\pm9$	$1201 \pm 16$
10	323.15	1	$69 \pm 14$	$8 \pm 3$	$5053 \pm 19$	$20 \pm 3$
10	348.15	1	$60 \pm 6$	$7 \pm 1$	$5029\pm7$	$49 \pm 6$
10	373.15	1	$53 \pm 4$	$8 \pm 1$	$4974\pm6$	$142 \pm 7$
10	398.15	1	$50 \pm 3$	$11 \pm 2$	$4882 \pm 5$	$312 \pm 9$
10	423.15	1	$49 \pm 2$	$11 \pm 1$	$4704\pm5$	$662 \pm 9$
30	323.15	1	$112 \pm 13$	$22 \pm 2$	$5087 \pm 15$	$13 \pm 4$
30	348.15	1	$98 \pm 3$	$08 \pm 3$ $24 \pm 5$ $5061 \pm 4$		$32 \pm 3$
30	373.15	1	$102 \pm 4$	$29 \pm 4$	$5041 \pm 6$	$67 \pm 5$
30	398.15	1	$105 \pm 4$	$32 \pm 3$	$4998\pm6$	$152 \pm 6$
30	423.15	1	$112 \pm 7$	$38 \pm 2$	$4926\pm8$	$297 \pm 4$
50	323.15	1	$120 \pm 6$	$37 \pm 6$	$5080\pm9$	$13 \pm 3$
50	348.15	1	$116 \pm 4$	$39 \pm 4$	$5069 \pm 2$	$25 \pm 3$
50	373.15	1	$121 \pm 5$	$46 \pm 5$	$5049 \pm 10$	$60 \pm 4$
50	398.15	1	$141 \pm 7$	$53 \pm 4$	$5029 \pm 6$	$127 \pm 10$
50	423.15	1	$148 \pm 5$	$60 \pm 6$	$4976 \pm 12$	$230 \pm 7$
5	323.15	2	$32 \pm 2$	$3\pm 2$	$5015 \pm 4$	$28 \pm 4$
5	348.15	2	$28 \pm 3$	$3\pm1$	$4981 \pm 2$	$87 \pm 6$
5	373.15	2	$25 \pm 2$	$3\pm1$	$4907\pm8$	$229 \pm 16$
5	398.15	2	$22 \pm 1$	$4 \pm 1$	$4738 \pm 3$	$558 \pm 4$
			Continued	l on next page		

p [MPa]	T [K]	$c_{\rm NaCl}$	$x_{\rm H_2} / [10^{-4}]$	$x_{\rm CO_2}$ / $[10^{-4}]$	$y_{\rm H_2}$ / [10 <sup>-4</sup> ]	$y_{\rm H_{2O}} / [10^{-4}]$
5	423.15	2	$22 \pm 1$	$4 \pm 1$	$4436 \pm 12$	$1156 \pm 23$
10	323.15	2	$51 \pm 3$	$6 \pm 2$	$5040 \pm 3$	$14 \pm 5$
10	348.15	2	$41 \pm 6$	$7 \pm 1$	$5008 \pm 6$	$54 \pm 7$
10	373.15	2	$45 \pm 5$	$6 \pm 1$	$4978 \pm 11$	$122 \pm 14$
10	398.15	2	$40 \pm 3$	$7 \pm 1$	$4878 \pm 7$	$308 \pm 10$
10	423.15	2	$39 \pm 4$	$10 \pm 1$	$4708 \pm 6$	$638 \pm 8$
30	323.15	2	$90 \pm 8$	$19 \pm 5$	$5067 \pm 11$	$13 \pm 4$
30	348.15	2	$84 \pm 8$	$18 \pm 3$	$5053 \pm 10$	$28 \pm 7$
30	373.15	2	$86 \pm 9$	$20 \pm 2$	$5032 \pm 8$	$70 \pm 4$
30	398.15	2	$89\pm7$	$26 \pm 3$	$4991\pm8$	$146 \pm 8$
30	423.15	2	$90 \pm 5$	$32 \pm 3$	$4913 \pm 8$	$291 \pm 10$
50	323.15	2	$99 \pm 6$	$35 \pm 7$	$5062 \pm 13$	$11 \pm 5$
50	348.15	2	$100 \pm 5$	$33 \pm 5$	$5053 \pm 8$	$33 \pm 4$
50	373.15	2	$98 \pm 4$	$37 \pm 1$	$5034 \pm 6$	$57 \pm 9$
50	398.15	2	$108 \pm 9$	$45 \pm 3$	$5003 \pm 13$	$125 \pm 10$
50	423.15	2	$119 \pm 6$	$52 \pm 2$	$4958 \pm 14$	$220 \pm 17$

p	Т	$c_{\rm NaCl}$	$\phi_{\mathrm{H}_2}$		$\phi_{ m CO_2}$		$\phi_{\mathrm{H_2O}}$	
[MPa]	[K]		CFCMC	RFP	CFCMC	RFP	CFCMC	RFP
5	323.15	0	$0.87 \pm 0.01$	0.86	$1.06 \pm 0.01$	1.07	$0.83 \pm 0.01$	0.86
5	348.15	0	$0.89 \pm 0.01$	0.89	$1.04 \pm 0.01$	1.06	$0.84 \pm 0.01$	0.89
5	373.15	0	$0.92 \pm 0.01$	0.91	$1.04 \pm 0.01$	1.06	$0.83 \pm 0.01$	0.90
5	398.15	0	$0.93 \pm 0.01$	0.93	$1.03 \pm 0.01$	1.06	$0.81 \pm 0.01$	0.91
5	423.15	0	$0.95 \pm 0.01$	0.94	$1.04 \pm 0.01$	1.06	$0.78 \pm 0.01$	0.91
10	323.15	0	$0.77 \pm 0.01$	0.75	$1.13 \pm 0.01$	1.16	$0.71 \pm 0.01$	0.75
10	348.15	0	$0.81 \pm 0.01$	0.80	$1.11 \pm 0.01$	1.13	$0.75 \pm 0.01$	0.79
10	373.15	0	$0.85 \pm 0.01$	0.84	$1.09 \pm 0.01$	1.12	$0.76 \pm 0.01$	0.83
10	398.15	0	$0.88 \pm 0.01$	0.87	$1.08 \pm 0.01$	1.11	$0.75 \pm 0.01$	0.85
10	423.15	0	$0.91 \pm 0.01$	0.89	$1.08 \pm 0.01$	1.10	$0.73 \pm 0.01$	0.86
30	323.15	0	$0.52 \pm 0.01$	0.49	$1.46 \pm 0.02$	1.50	$0.41 \pm 0.01$	0.48
30	348.15	0	$0.61 \pm 0.01$	0.58	$1.38 \pm 0.02$	1.42	$0.50 \pm 0.01$	0.56
30	373.15	0	$0.70 \pm 0.01$	0.66	$1.33 \pm 0.01$	1.36	$0.56 \pm 0.01$	0.63
30	398.15	0	$0.76 \pm 0.01$	0.72	$1.29 \pm 0.01$	1.32	$0.59\pm0.01$	0.68
30	423.15	0	$0.81 \pm 0.01$	0.77	$1.26 \pm 0.01$	1.29	$0.59 \pm 0.01$	0.71
50	323.15	0	$0.44 \pm 0.01$	0.42	$1.77 \pm 0.03$	1.81	$0.29 \pm 0.01$	0.38
50	348.15	0	$0.55 \pm 0.01$	0.52	$1.65 \pm 0.01$	1.69	$0.38 \pm 0.01$	0.47
50	373.15	0	$0.64 \pm 0.01$	0.60	$1.56 \pm 0.01$	1.60	$0.44 \pm 0.01$	0.54
50	398.15	0	$0.72 \pm 0.01$	0.68	$1.51 \pm 0.01$	1.54	$0.49 \pm 0.01$	0.60
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Table S7: The fugacity coefficients ( $\phi$ ) of all species in the gas-rich phase obtained from CFCMC simulations<sup>24–26</sup> are compared to the corresponding values from REFPROP (RFP). Fugacity coefficients from REFPROP for H<sub>2</sub>, CO<sub>2</sub> and H<sub>2</sub>O at given pressure, and temperature are obtained at the gas-phase composition obtained from CFCMC simulations.

p	Т	$c_{\rm NaCl}$	$\phi_{\mathrm{H}_2}$		$\phi_{\rm CO_2}$		$\phi_{\mathrm{H_2O}}$	
[MPa]	[K]		CFCMC	RFP	CFCMC	RFP	CFCMC	RFP
50	423.15	0	$0.79\pm0.01$	0.74	$1.45 \pm 0.01$	1.48	$0.51\pm0.01$	0.65
5	323.15	1	$0.87 \pm 0.01$	0.86	$1.06 \pm 0.01$	1.07	$0.83 \pm 0.01$	0.86
5	348.15	1	$0.89 \pm 0.01$	0.89	$1.04 \pm 0.01$	1.06	$0.84 \pm 0.01$	0.89
5	373.15	1	$0.91 \pm 0.01$	0.91	$1.03 \pm 0.01$	1.06	$0.83 \pm 0.01$	0.90
5	398.15	1	$0.93 \pm 0.01$	0.93	$1.04 \pm 0.01$	1.05	$0.82 \pm 0.01$	0.91
5	423.15	1	$0.95 \pm 0.01$	0.94	$1.04 \pm 0.01$	1.06	$0.78 \pm 0.01$	0.91
10	323.15	1	$0.76 \pm 0.01$	0.75	$1.12 \pm 0.02$	1.16	$0.70 \pm 0.01$	0.75
10	348.15	1	$0.82 \pm 0.01$	0.80	$1.11 \pm 0.01$	1.13	$0.75 \pm 0.01$	0.79
10	373.15	1	$0.86 \pm 0.01$	0.84	$1.11 \pm 0.01$	1.12	$0.77 \pm 0.01$	0.83
10	398.15	1	$0.88 \pm 0.01$	0.87	$1.08 \pm 0.01$	1.11	$0.76 \pm 0.01$	0.85
10	423.15	1	$0.91 \pm 0.01$	0.89	$1.09 \pm 0.01$	1.10	$0.74 \pm 0.01$	0.86
30	323.15	1	$0.52 \pm 0.01$	0.49	$1.47 \pm 0.01$	1.51	$0.41 \pm 0.01$	0.47
30	348.15	1	$0.61 \pm 0.01$	0.58	$1.39 \pm 0.01$	1.43	$0.50 \pm 0.01$	0.56
30	373.15	1	$0.69 \pm 0.01$	0.65	$1.33 \pm 0.01$	1.37	$0.56 \pm 0.01$	0.62
30	398.15	1	$0.76 \pm 0.01$	0.72	$1.29 \pm 0.01$	1.33	$0.59 \pm 0.01$	0.68
30	423.15	1	$0.82 \pm 0.01$	0.77	$1.27 \pm 0.01$	1.30	$0.60 \pm 0.01$	0.71
50	323.15	1	$0.44 \pm 0.01$	0.42	$1.78 \pm 0.01$	1.81	$0.29 \pm 0.01$	0.38
50	348.15	1	$0.54 \pm 0.01$	0.51	$1.66 \pm 0.01$	1.70	$0.38 \pm 0.01$	0.46
50	373.15	1	$0.64 \pm 0.01$	0.60	$1.57 \pm 0.01$	1.61	$0.45 \pm 0.01$	0.54
50	398.15	1	$0.72 \pm 0.01$	0.68	$1.50 \pm 0.01$	1.54	$0.49 \pm 0.01$	0.60
50	423.15	1	$0.79 \pm 0.01$	0.74	$1.45 \pm 0.01$	1.49	$0.51 \pm 0.01$	0.65
5	323.15	2	$0.86 \pm 0.01$	0.86	$1.05 \pm 0.01$	1.07	$0.82 \pm 0.01$	0.86
5	348.15	2	$0.89 \pm 0.01$	0.89	$1.05 \pm 0.01$	1.06	$0.84 \pm 0.01$	0.89
			Contin	ued on	next page			

p	Т	$c_{ m NaCl}$	$\phi_{\mathrm{H}_2}$		$\phi_{\rm CO_2}$		$\phi_{\mathrm{H_2O}}$	
[MPa]	[K]		CFCMC	RFP	CFCMC	RFP	CFCMC	RFP
5	373.15	2	$0.91 \pm 0.01$	0.91	$1.04 \pm 0.01$	1.06	$0.84 \pm 0.01$	0.90
5	398.15	2	$0.93 \pm 0.01$	0.93	$1.04 \pm 0.01$	1.05	$0.82 \pm 0.01$	0.91
5	423.15	2	$0.95\pm0.01$	0.94	$1.04 \pm 0.01$	1.06	$0.79\pm0.01$	0.91
10	323.15	2	$0.76 \pm 0.01$	0.75	$1.13 \pm 0.01$	1.16	$0.71 \pm 0.01$	0.75
10	348.15	2	$0.82 \pm 0.01$	0.80	$1.12 \pm 0.01$	1.13	$0.76 \pm 0.01$	0.79
10	373.15	2	$0.85 \pm 0.01$	0.84	$1.10 \pm 0.01$	1.12	$0.77 \pm 0.01$	0.83
10	398.15	2	$0.88 \pm 0.01$	0.87	$1.09 \pm 0.01$	1.11	$0.76 \pm 0.01$	0.85
10	423.15	2	$0.91 \pm 0.01$	0.89	$1.08 \pm 0.01$	1.10	$0.74 \pm 0.01$	0.86
30	323.15	2	$0.52 \pm 0.01$	0.49	$1.48 \pm 0.01$	1.51	$0.41 \pm 0.01$	0.47
30	348.15	2	$0.62 \pm 0.01$	0.58	$1.39 \pm 0.01$	1.43	$0.50 \pm 0.01$	0.56
30	373.15	2	$0.69 \pm 0.01$	0.65	$1.33 \pm 0.02$	1.37	$0.56 \pm 0.01$	0.62
30	398.15	2	$0.76 \pm 0.01$	0.72	$1.29 \pm 0.01$	1.33	$0.60 \pm 0.01$	0.68
30	423.15	2	$0.81 \pm 0.01$	0.77	$1.26 \pm 0.01$	1.30	$0.60 \pm 0.01$	0.71
50	323.15	2	$0.44 \pm 0.01$	0.42	$1.77 \pm 0.01$	1.82	$0.29 \pm 0.01$	0.38
50	348.15	2	$0.54 \pm 0.01$	0.51	$1.66 \pm 0.01$	1.70	$0.37 \pm 0.01$	0.46
50	373.15	2	$0.63 \pm 0.01$	0.60	$1.57 \pm 0.01$	1.61	$0.45 \pm 0.01$	0.54
50	398.15	2	$0.72 \pm 0.01$	0.67	$1.50 \pm 0.01$	1.54	$0.49 \pm 0.01$	0.60
50	423.15	2	$0.78 \pm 0.01$	0.74	$1.45 \pm 0.01$	1.49	$0.52 \pm 0.01$	0.65

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